

Faculty of Mechanical Science and Engineering
Chair of Computational and Experimental Solid Mechanics

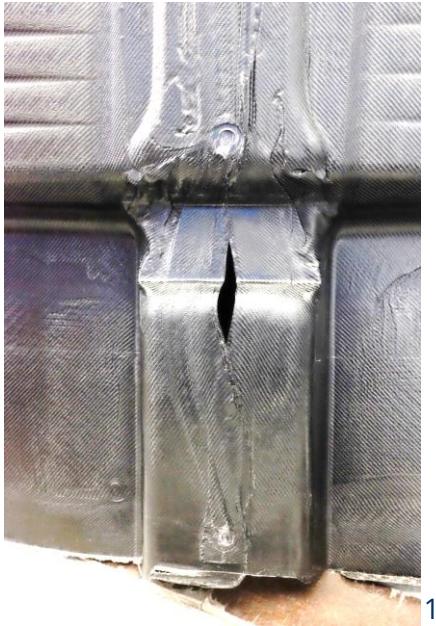
Jean-Paul Ziegs

Numerical Modeling of Single-Step Thermoforming of a Hybrid Metal/FRP Lightweight Structure

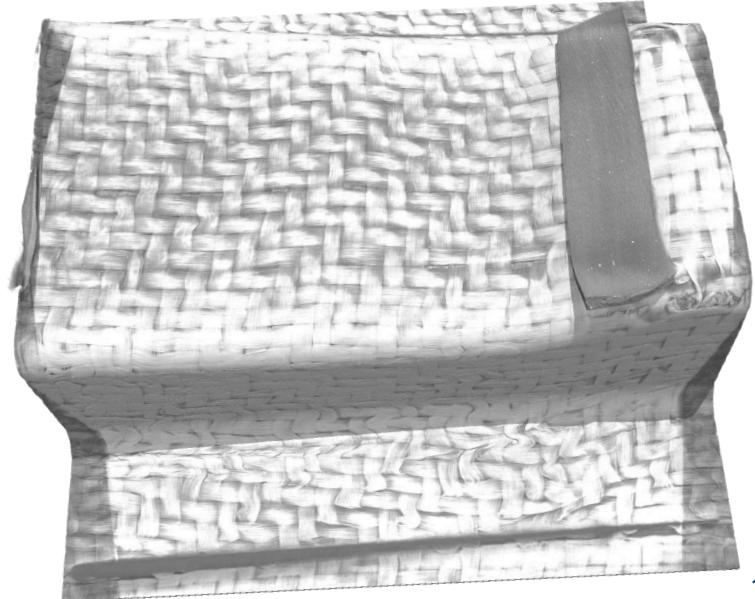
15th German LS-DYNA Forum 2018 // Bamberg // 15.-17.10.2018



- Manufacturing process of hybrid workpieces characterized by “trial and error”



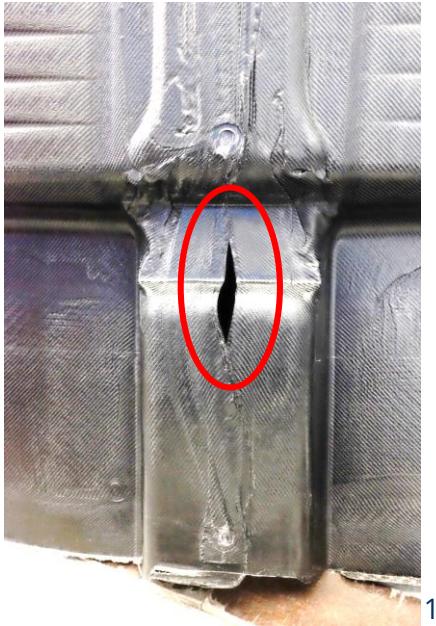
1)



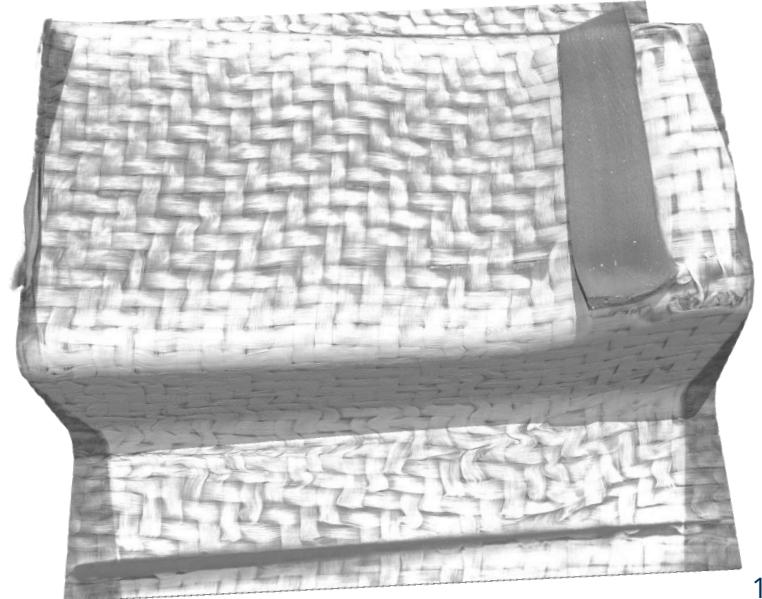
1)

1) TU Dresden, ILK

- Manufacturing process of hybrid workpieces characterized by “trial and error”



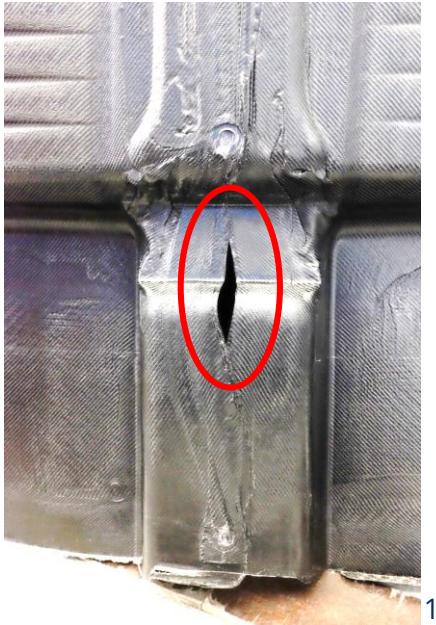
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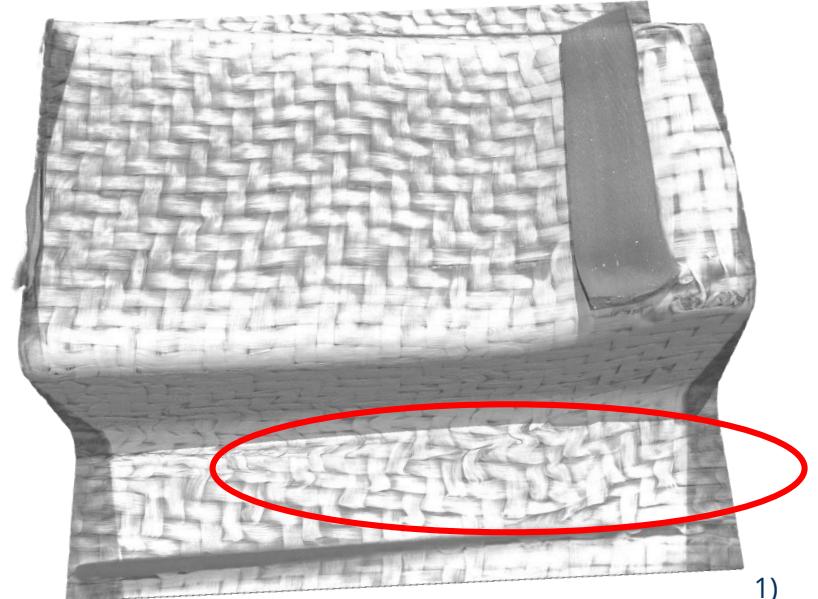
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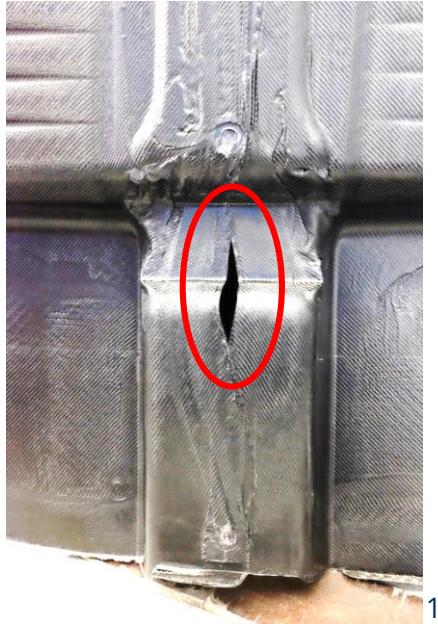
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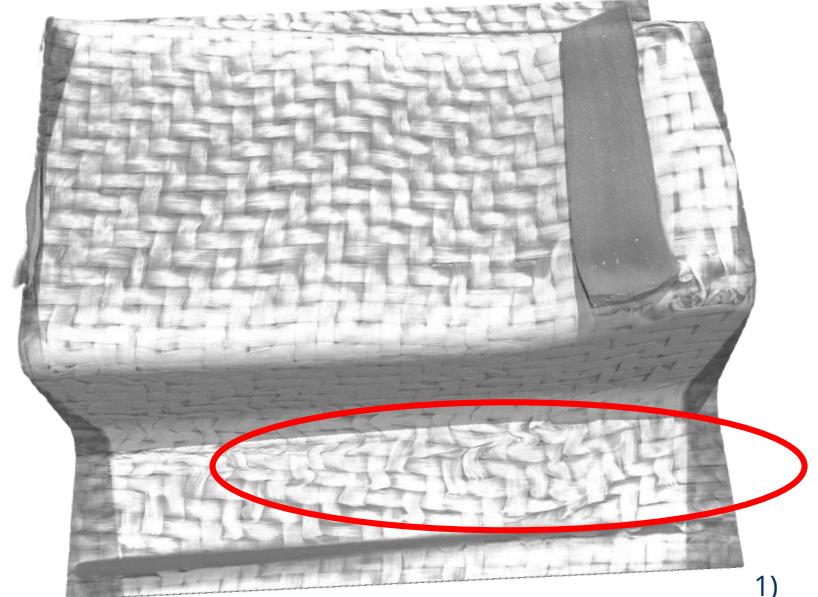
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1) TU Dresden, ILK

- Manufacturing process of hybrid workpieces characterized by “trial and error”



1)



1)

- Simulation of manufacturing processes to optimize process parameters

1) TU Dresden, ILK

Introduction and motivation

Process chain

Material modeling and parametrization

Process simulation and results

Summary

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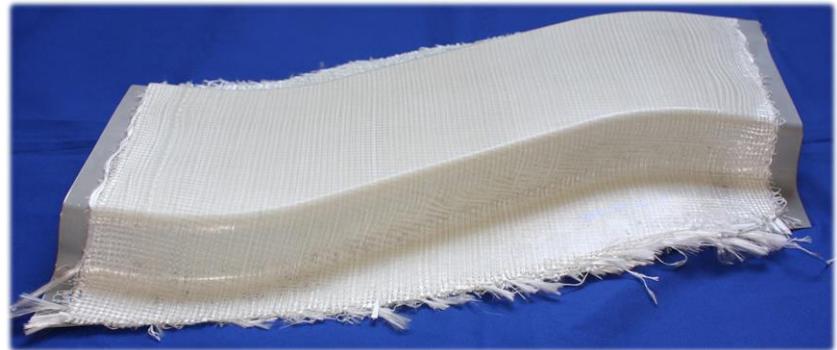
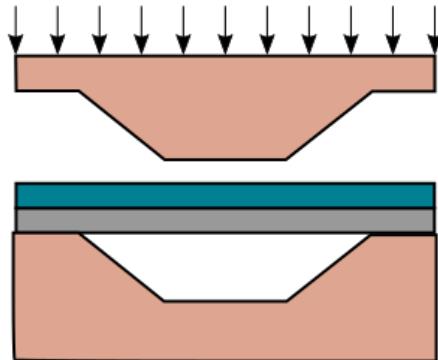
Material modeling and parametrization

Process simulation and results

Summary

Process chain

Manufacturing process

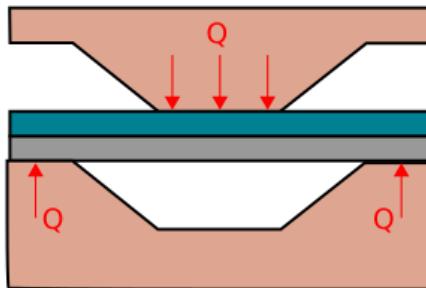


2)

2) TU Dresden, IF

Process chain

Manufacturing process

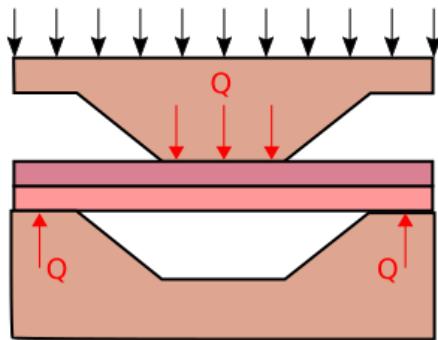


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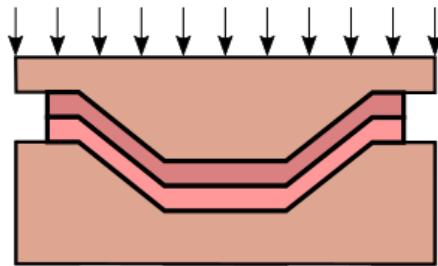


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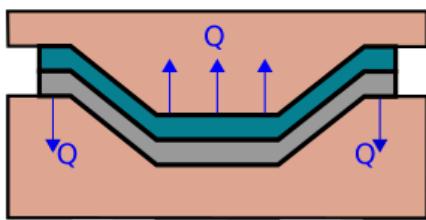


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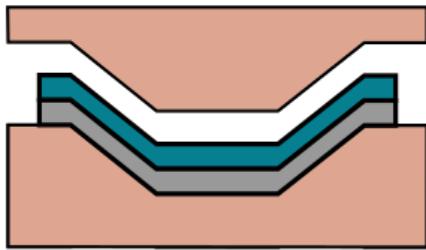


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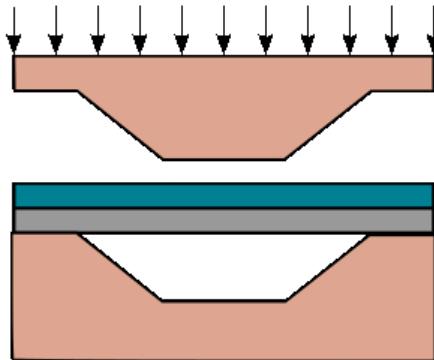


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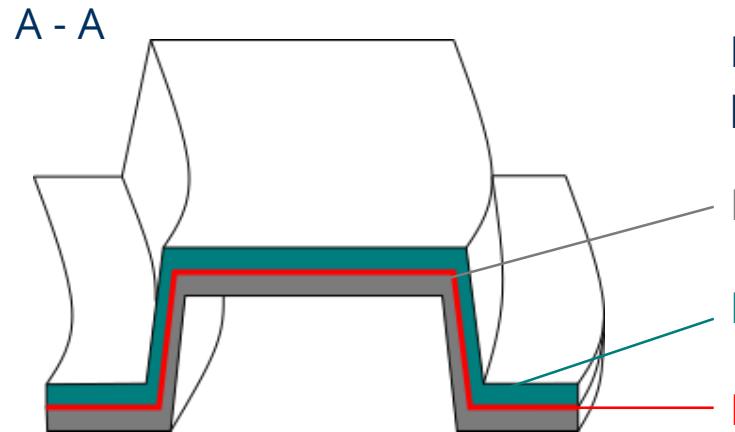
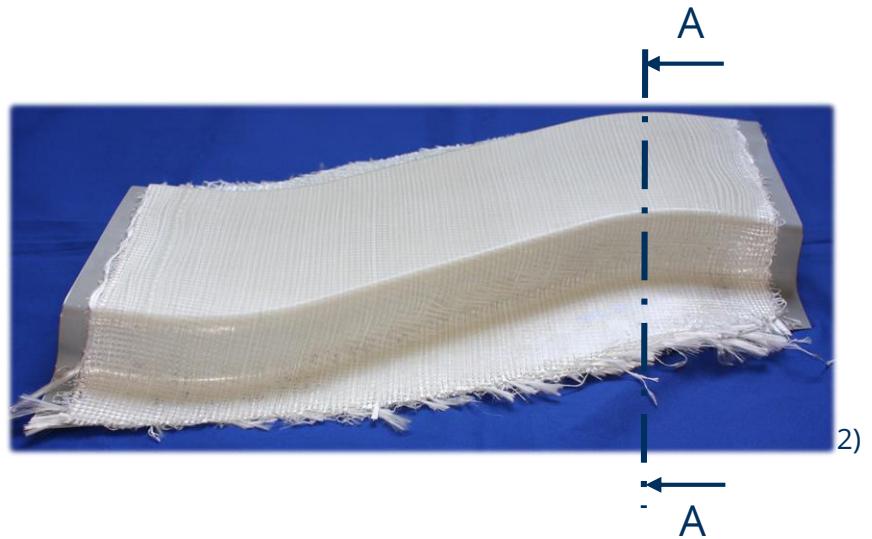
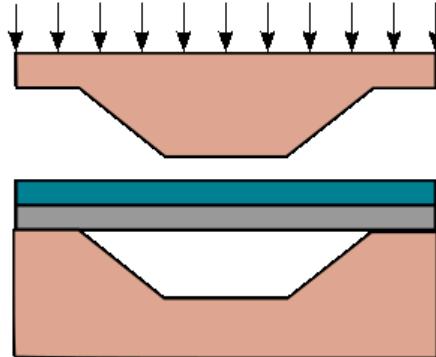


2)

2) TU Dresden, IF

Process chain

Manufacturing process



Material modeling to predict behavior of:

Metal

Fiber-reinforced plastic

Interface

2) TU Dresden, IF

Material modeling and parametrization

➤ Metal (*MAT122-HILL_3R)

Metal sheet: DC05



Constitutive law:

- Anisotropic elastic-plastic
- HILL48-yield criterion
- Temperature independent

Uniaxial tension tests for parameter identification



3) ThyssenKrupp-Company presentation, February 2013

Material modeling and parametrization

➤ Metal (*MAT122-Hill_3R)

Metal sheet: DC05



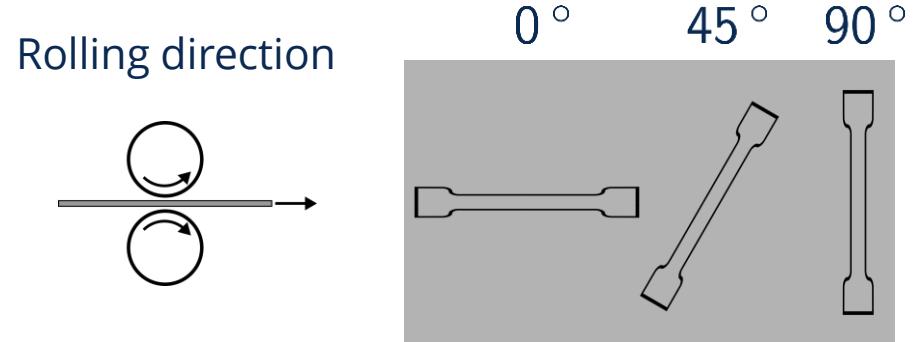
Constitutive law:

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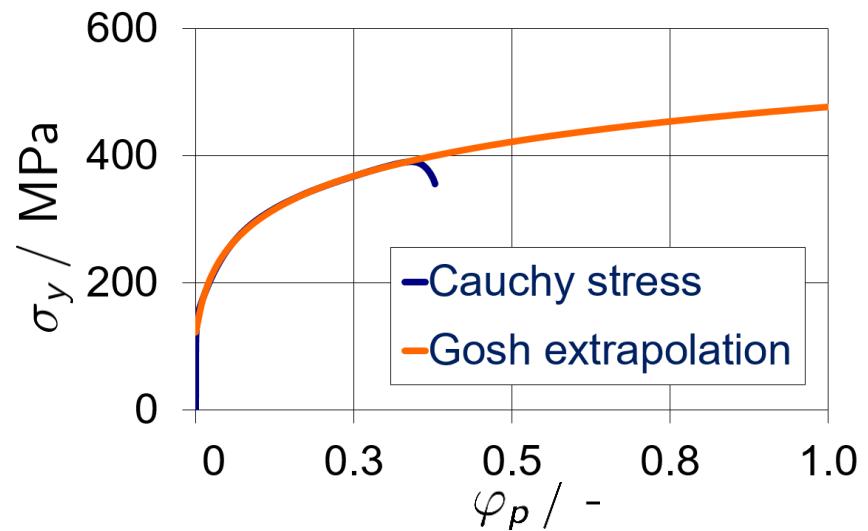
Uniaxial tension tests for parameter identification



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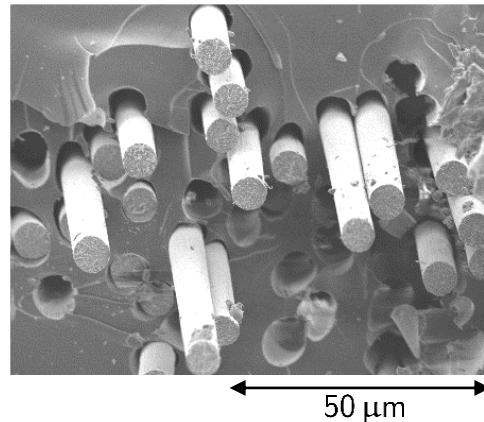
Parameter	E	ν	R_{00}	R_{45}	R_{90}
Value	207 GPa	0.28	1.88	1.4	2.23



Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

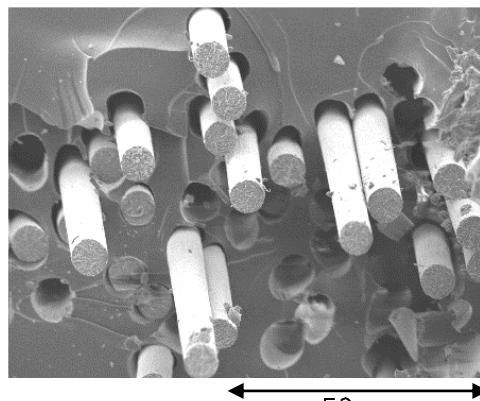
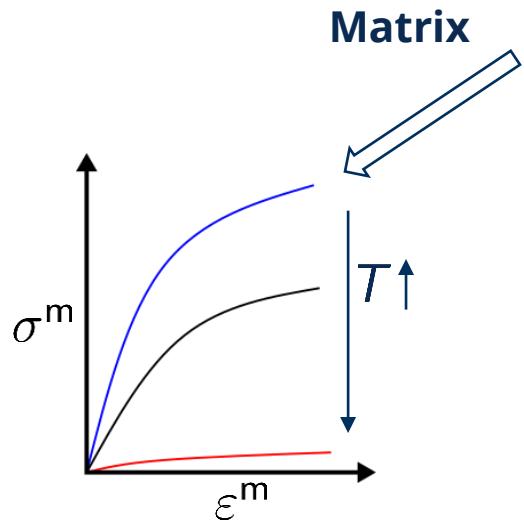
FRP material: CF-PA6.6



Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

FRP material: CF-PA6.6

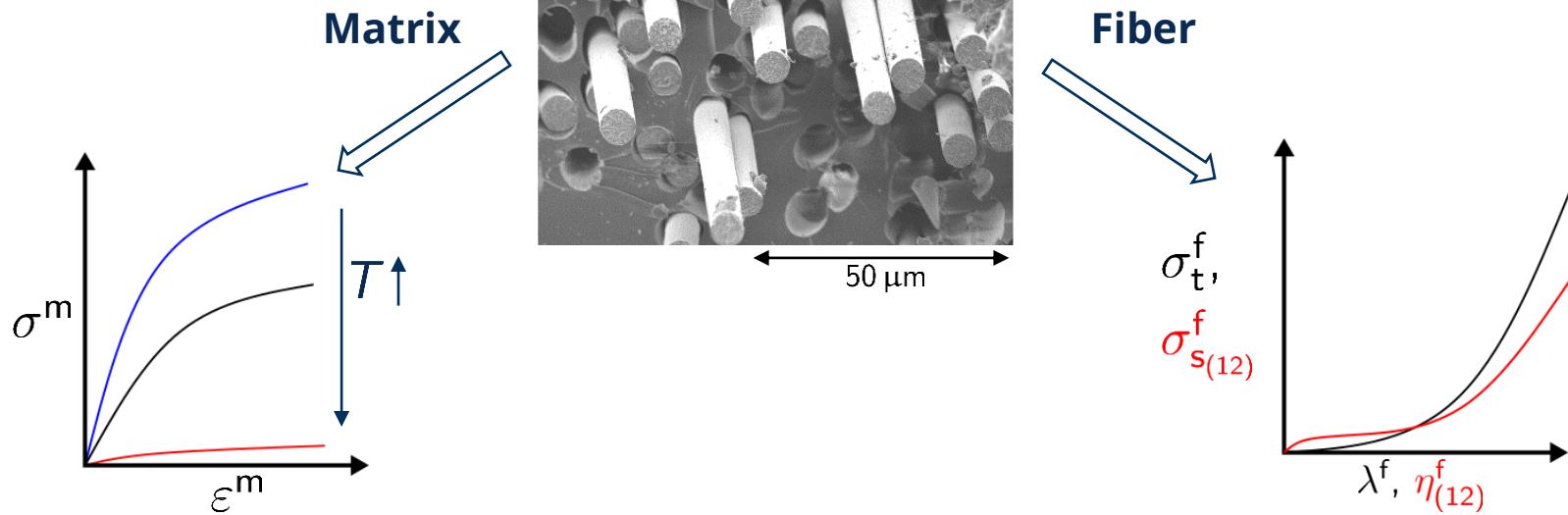


- Thermo-elastic-plastic
- V. Mises-yield criterion
- Vanishing stiffness and yield stress at melting temperature

Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

FRP material: CF-PA6.6



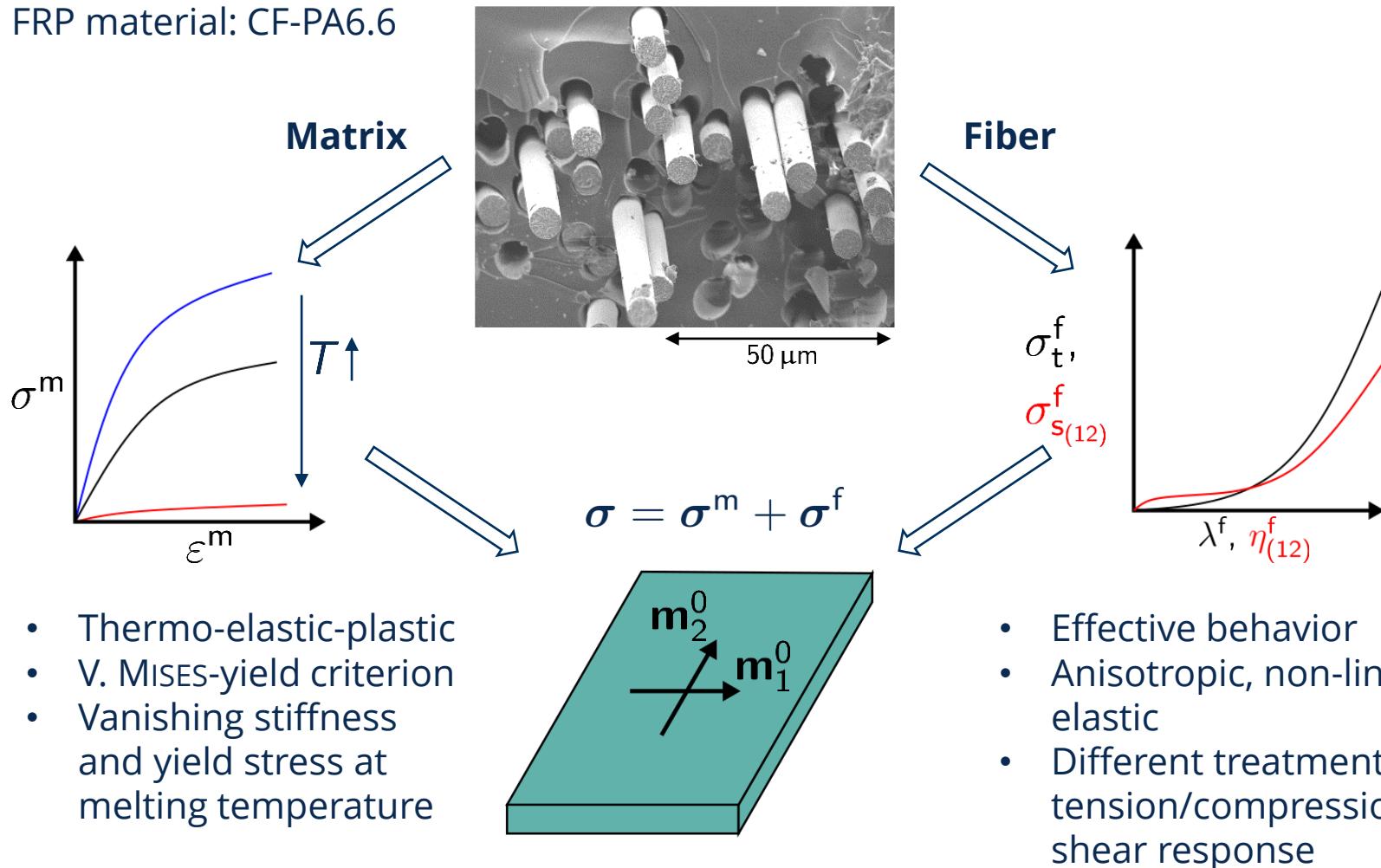
- Thermo-elastic-plastic
- V. Mises-yield criterion
- Vanishing stiffness and yield stress at melting temperature

- Effective behavior
- Anisotropic, non-linear elastic
- Different treatments for tension/compression and shear response

Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

FRP material: CF-PA6.6

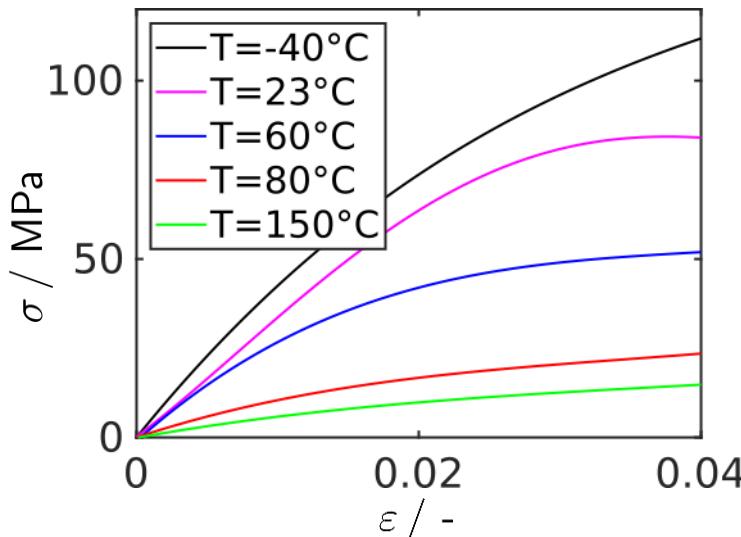


Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

Temperature dependent material behavior of polyamide 6.6 (PA6.6)

Stress-strain curves ($-40^{\circ}\text{C} < T < 150^{\circ}\text{C}$)
of PA 6.6 from database: "Campusplastics"



- Determination of stiffnesses and initial yield stresses by EHRENSTEIN⁴⁾
- Empirical extrapolation approach⁵⁾ for flow rules at higher temperatures

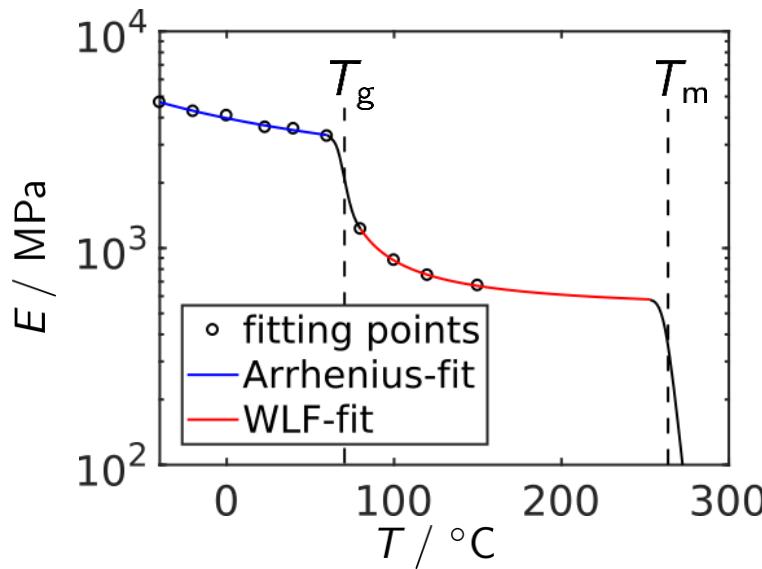
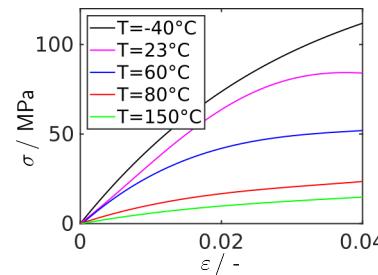
4) Ehrenstein 2001 5) Behrens et al. 2015

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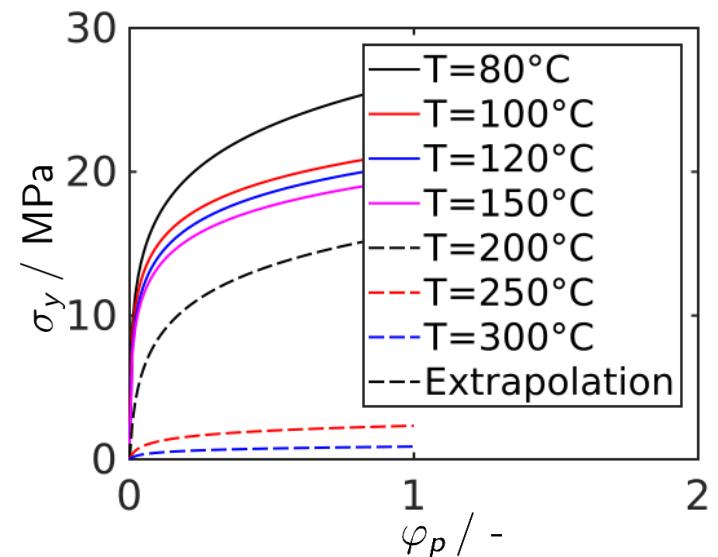
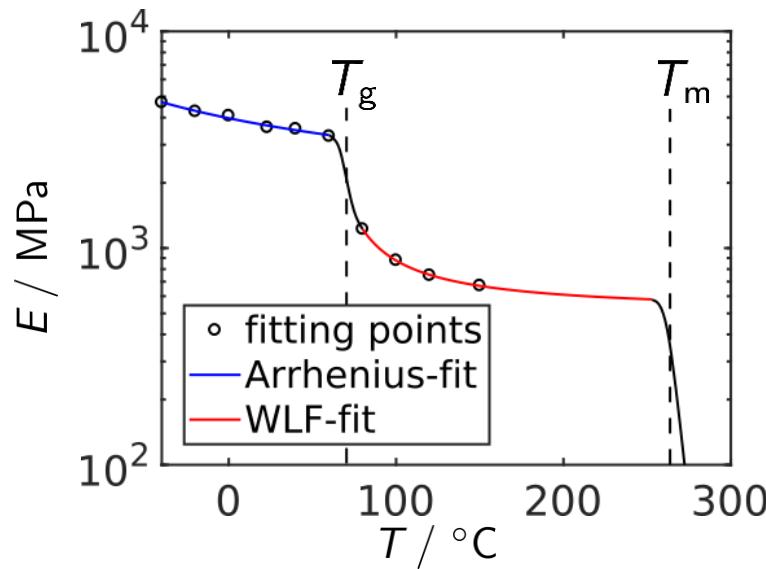
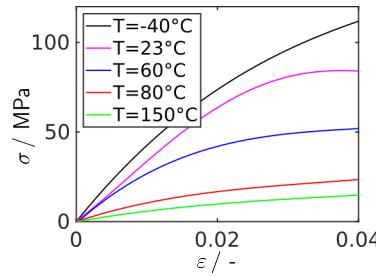
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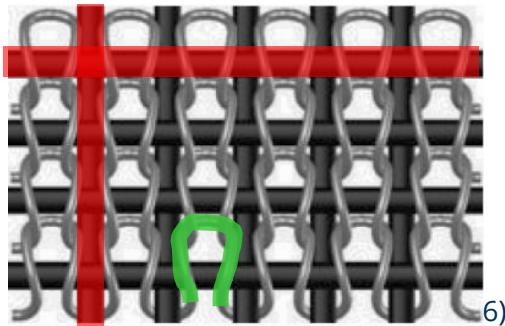
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Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

Textile material:
biaxial reinforced
weft-knitted fabric



Reinforcement yarns:
carbon fiber (CF) &
polyamide 6.6 (PA6.6)

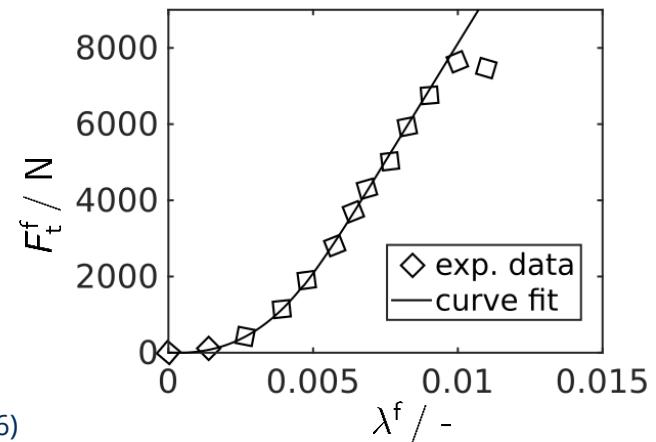
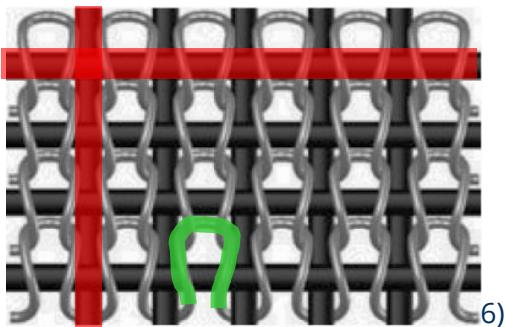
Knitting yarns:
glass fiber (GF) & PA6.6

6) TU Dresden, ITM

Material modeling and parametrization

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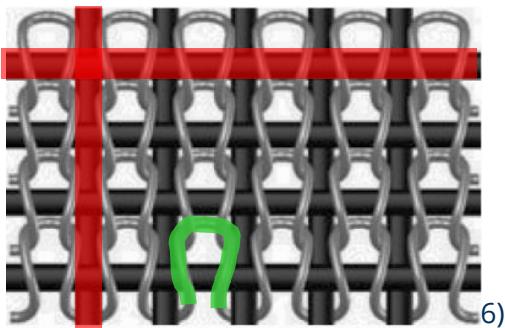
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Material modeling and parametrization

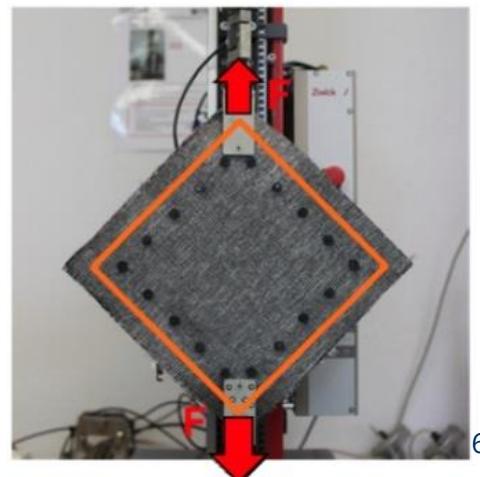
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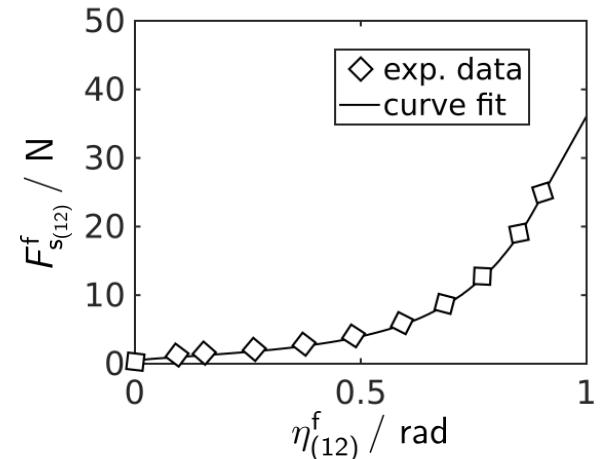
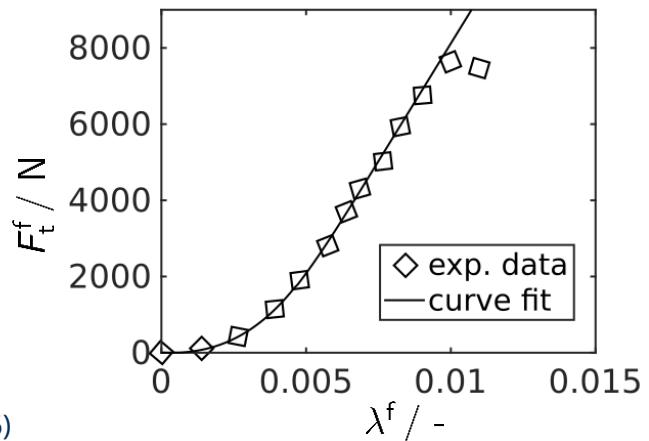
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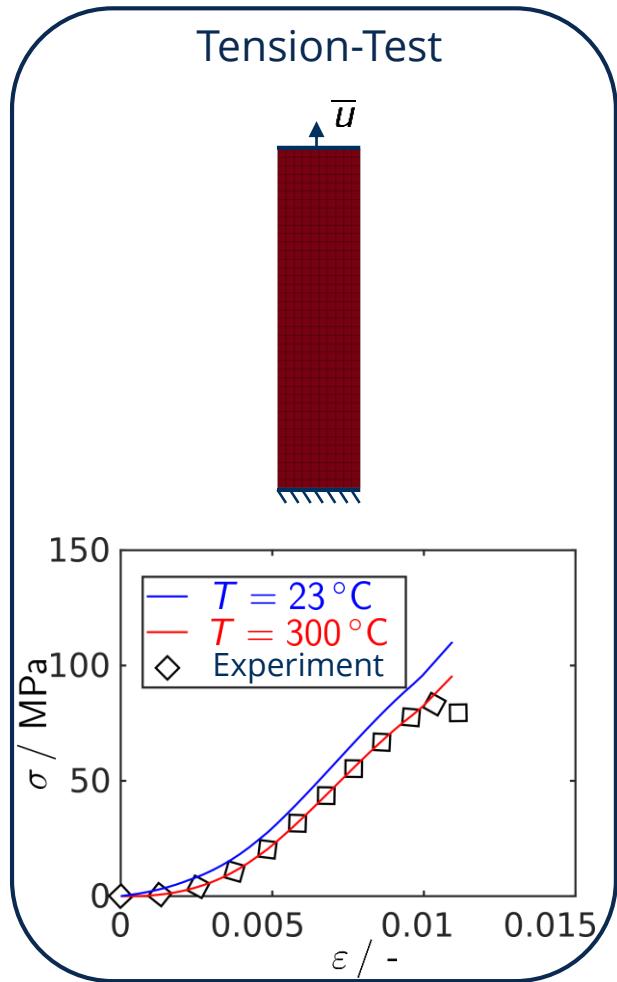
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Material modeling and parametrization

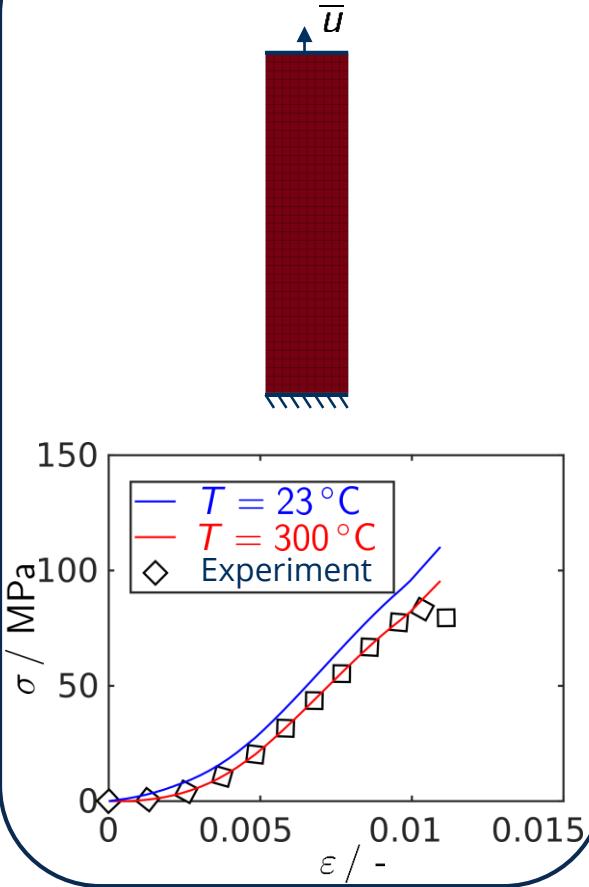
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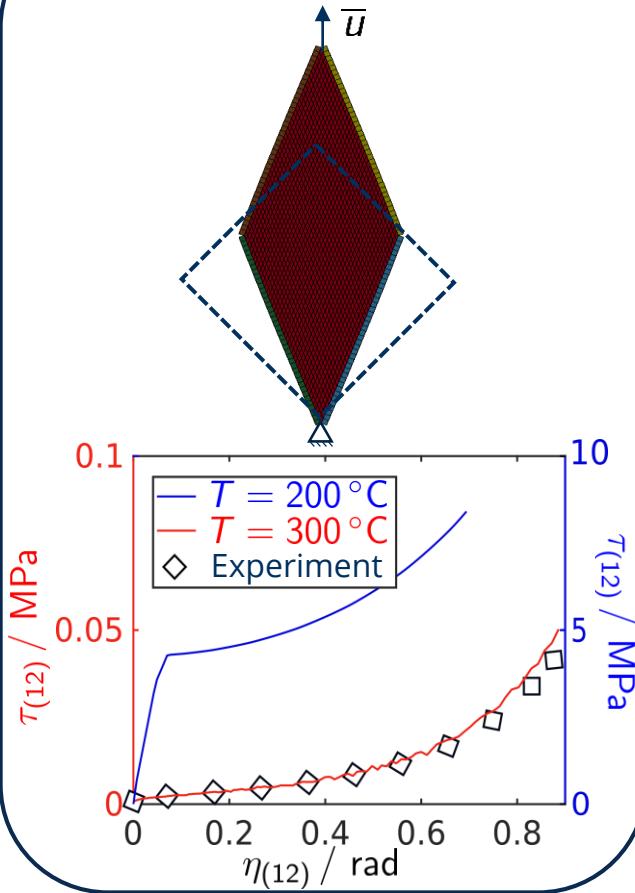
Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

Tension-Test



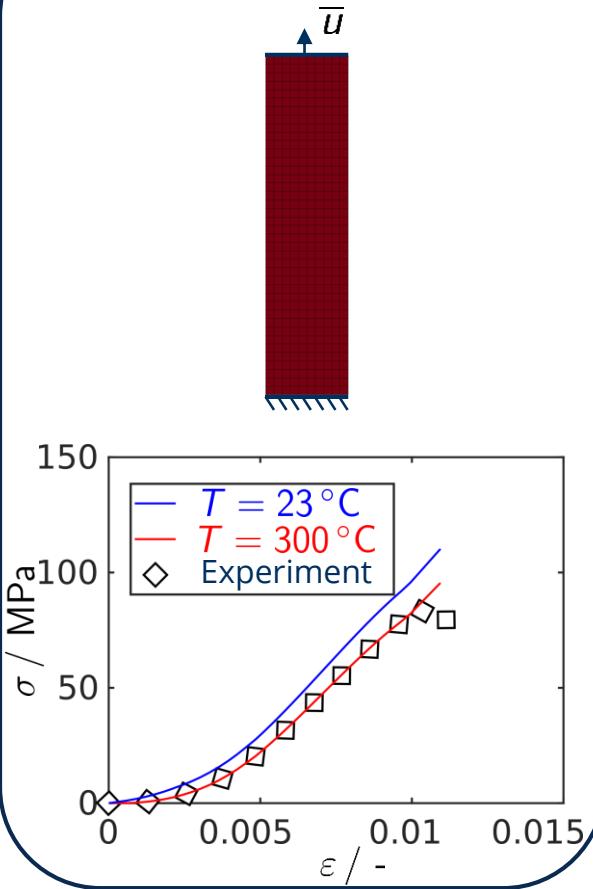
Picture-Frame-Test



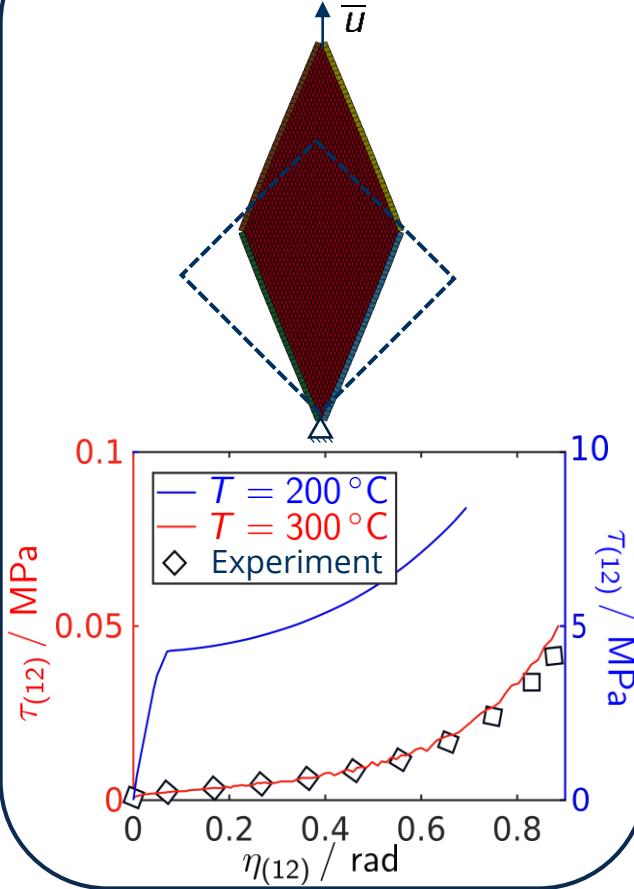
Material modeling and parametrization

➤ FRP (*MAT249-Reinforced_Thermoplastic)

Tension-Test



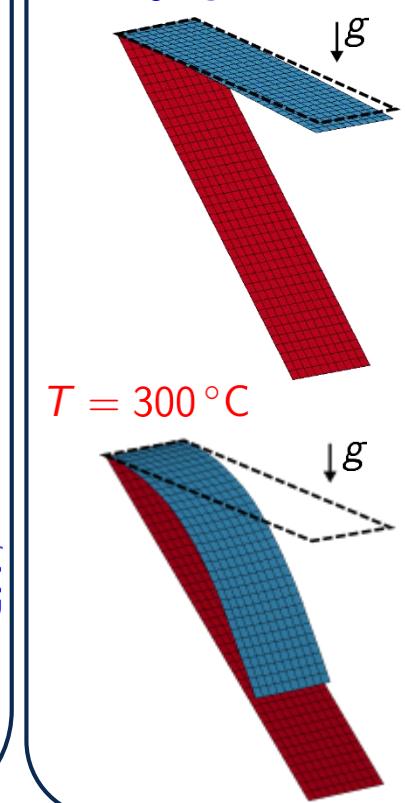
Picture-Frame-Test



Cantilever-Test

$T = 23^\circ\text{C}$

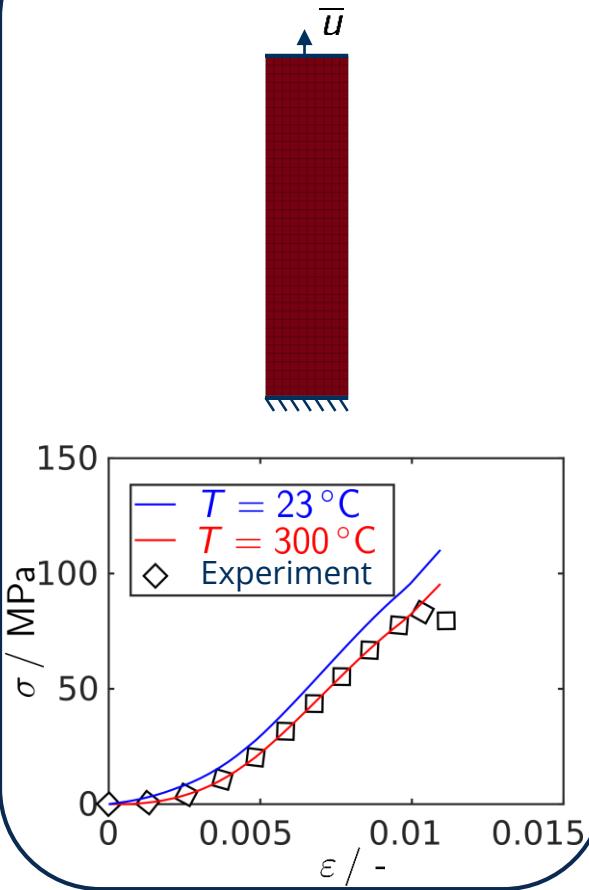
$T = 300^\circ\text{C}$



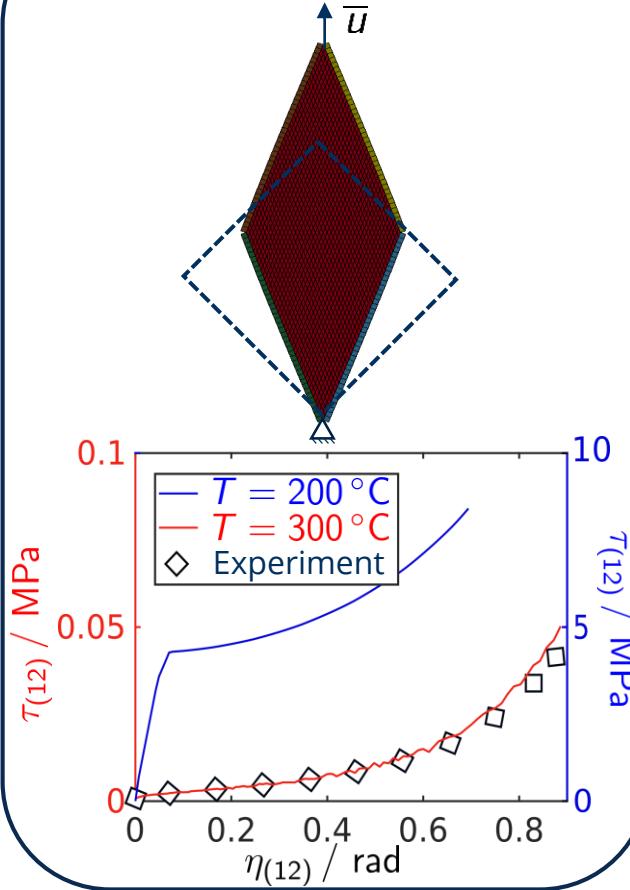
Material modeling and parametrization

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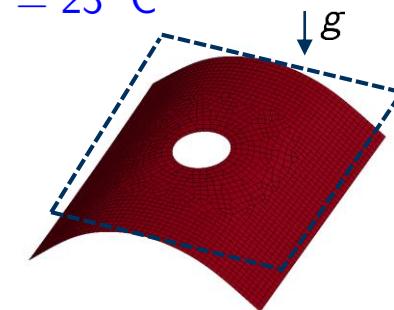


Picture-Frame-Test

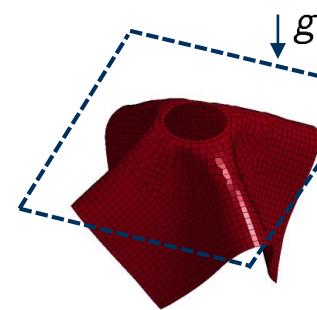


Multiaxial bending

$T = 23^\circ\text{C}$



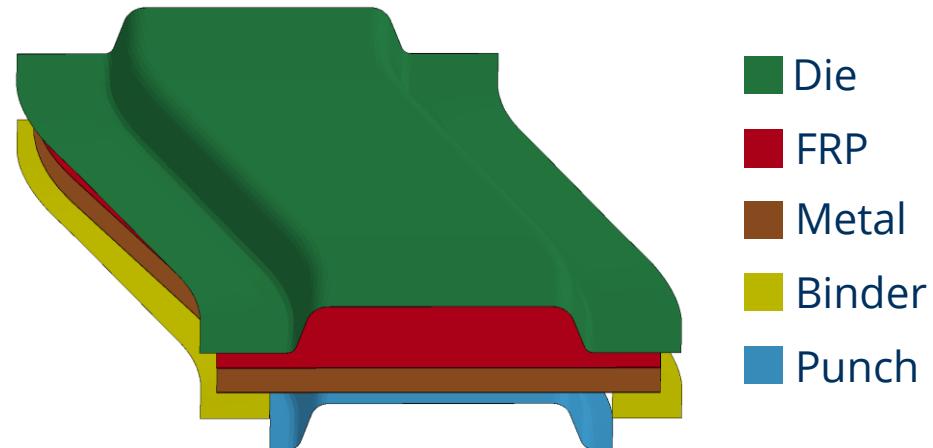
$T = 300^\circ\text{C}$



Process simulation and results

➤ Process modeling

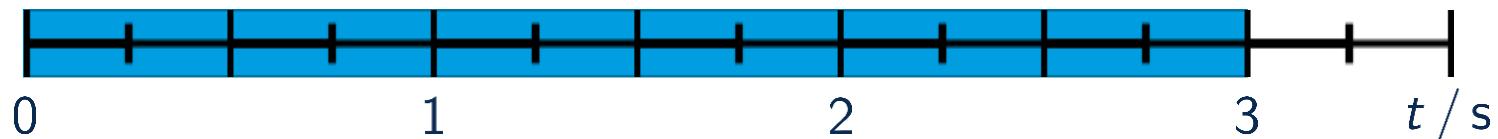
Parameter	Value
T_0^{FRP}	300 °C
T_0^{Metal}	220 °C
T^{Tool}	150 °C (const.)
t_{Process}	3 s
n_{Elements}	$\approx 2 \cdot 40000$
h_{Elements}	$\approx 2 \text{ mm}$
Δt_{mech}	$\approx 1 \cdot 10^{-6} \text{ s}$
Δt_{therm}	$\approx 1 \cdot 10^{-4} \text{ s}$



Step 1: Heating

Step 2: Forming

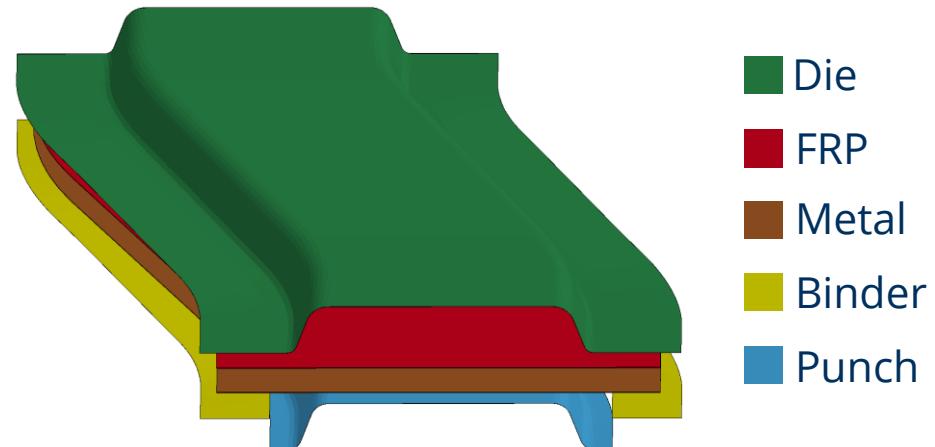
Step 3: Cooling



Process simulation and results

➤ Process modeling

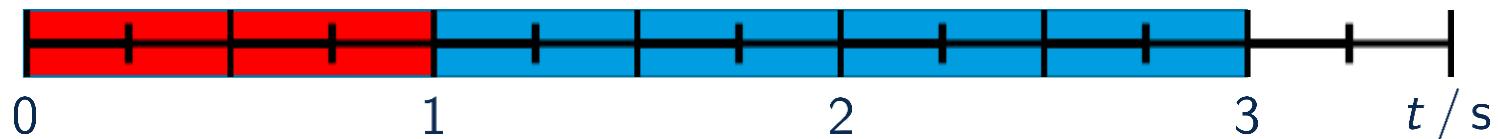
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Step 2: Forming

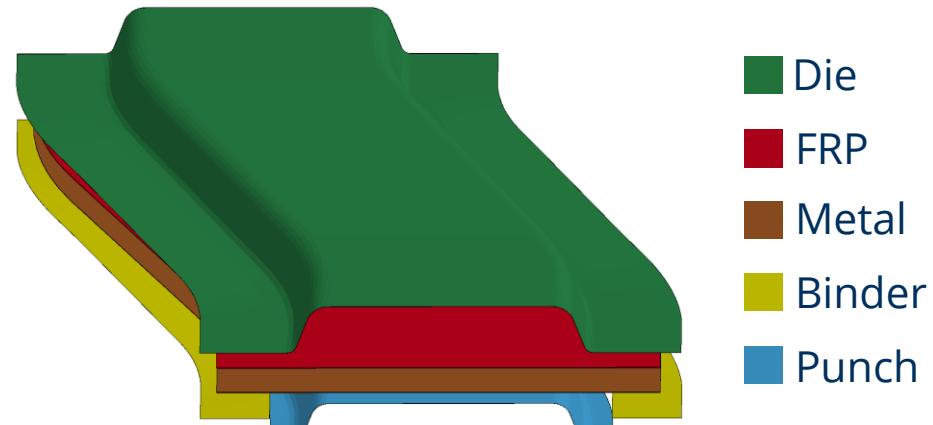
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Process simulation and results

➤ Process modeling

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Step 2: Forming

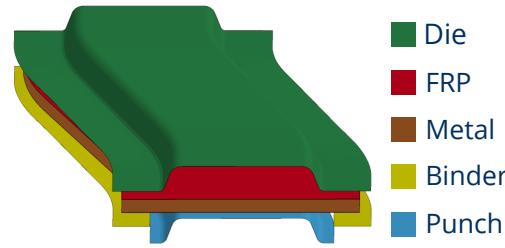
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Process simulation and results

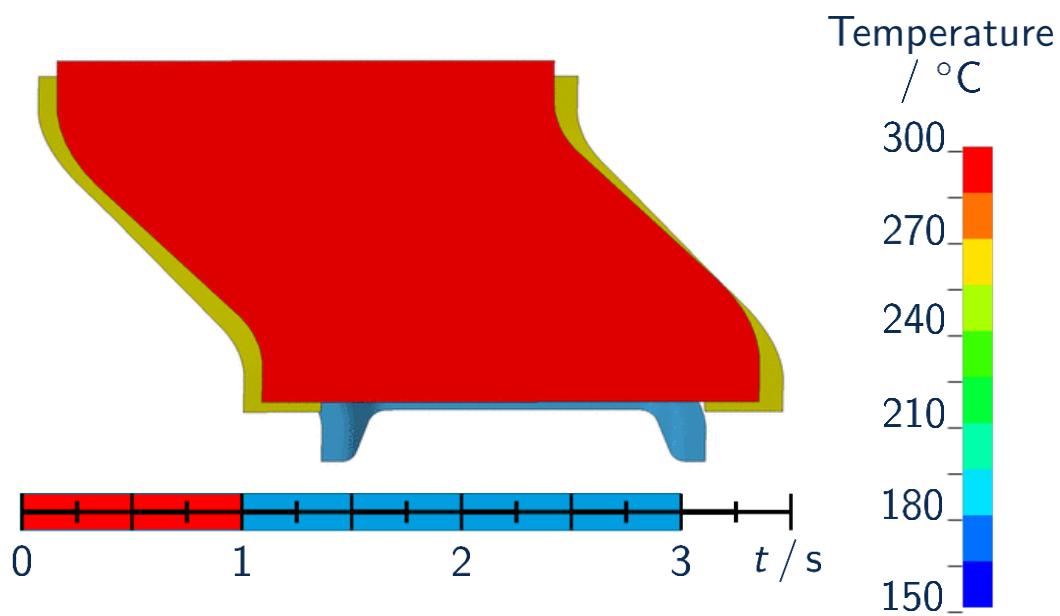
➤ Process modeling and results

Parameter	Value
t_{Forming}	1 s
v_{Punch}	50 mm/s
F_{Binder}	10 kN
t_{Holding}	2 s



Parameter	Value
μ, μ_0	0.15
h_{cont}	1000 W/m ² K
L_{\min}	1 mm

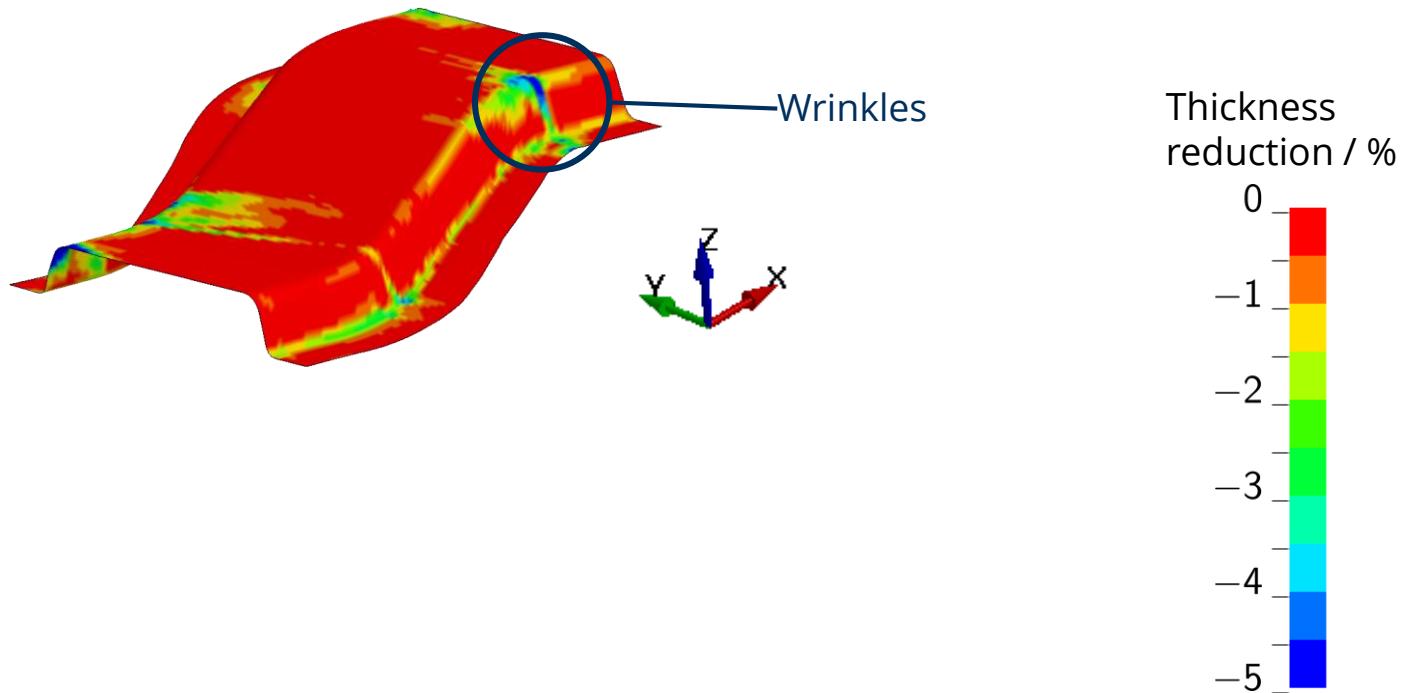
Parameter	Value
c_p^{FRP}	1.7 J/gK
k^{FRP}	0.23 W/mK
$\alpha_{\text{th}}^{\text{FRP}}$	$0.3 \cdot 10^{-6} \text{ K}^{-1}$
c_p^{DC05}	460 J/gK
k^{DC05}	50 W/mK
$\alpha_{\text{th}}^{\text{DC05}}$	$1 \cdot 10^{-6} \text{ K}^{-1}$



Process simulation and results

➤ Results

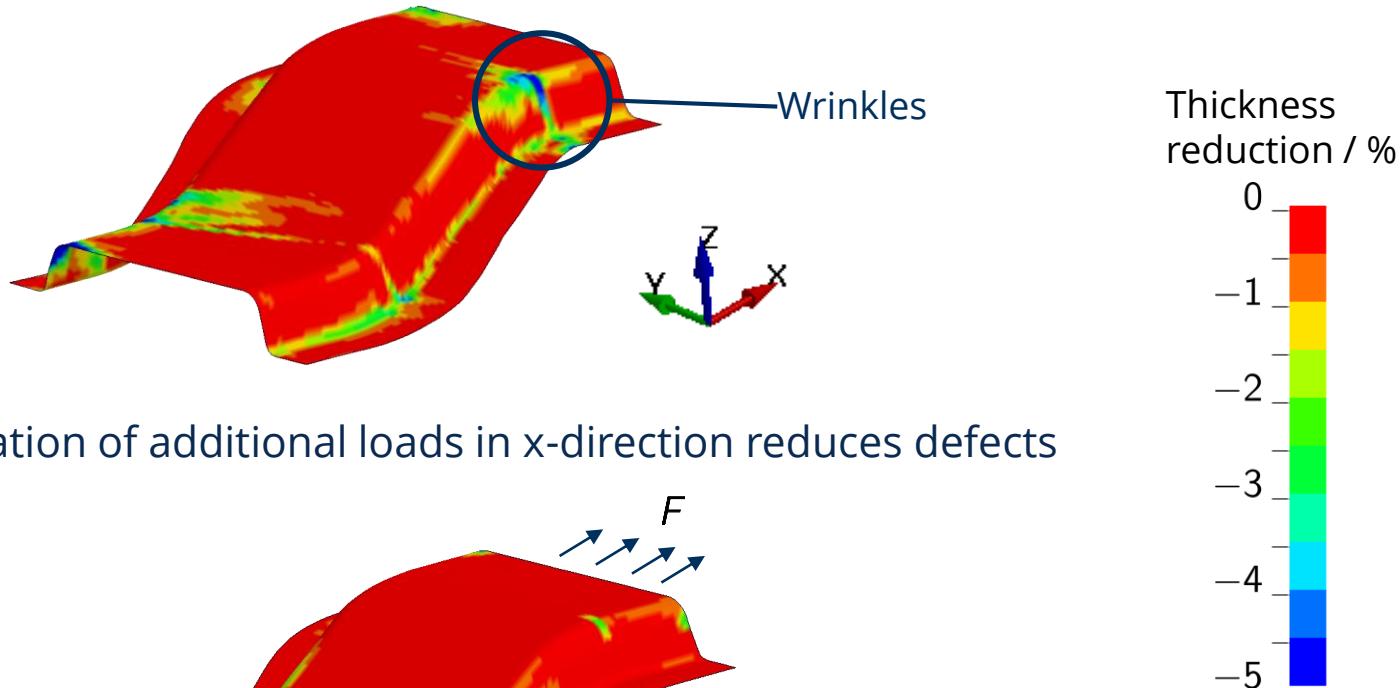
Formation of wrinkles due to missing tensile forces in x-direction



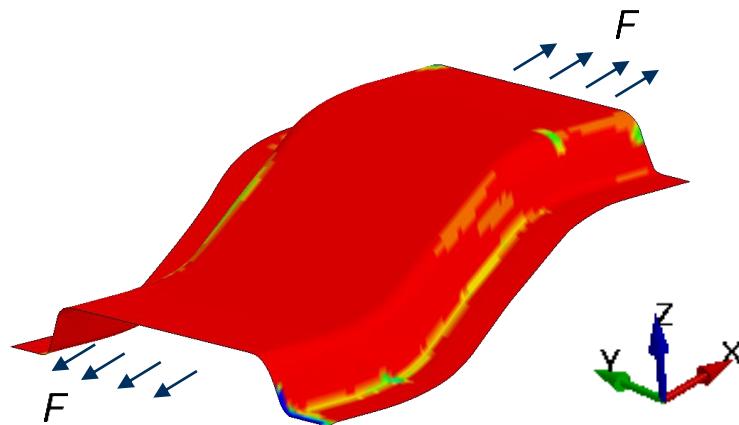
Process simulation and results

➤ Results

Formation of wrinkles due to missing tensile forces in x-direction

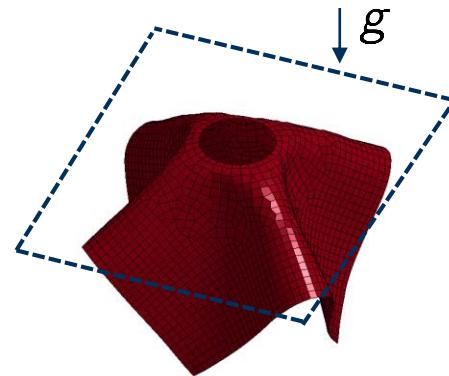


Application of additional loads in x-direction reduces defects



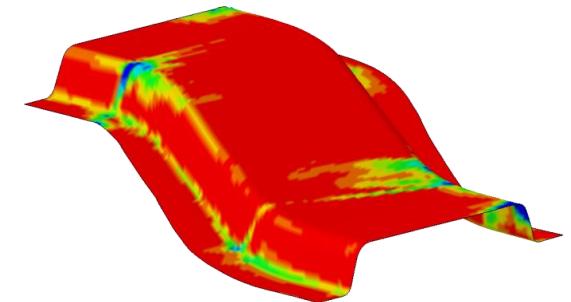
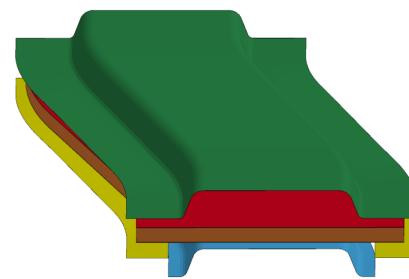
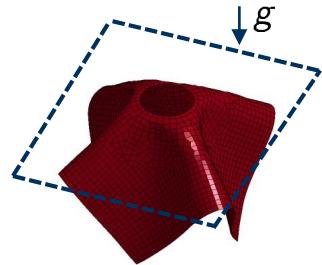
Summary

- ✓ Formulation for temperature dependent forming behavior of pre-consolidated fiber-reinforced thermoplastics



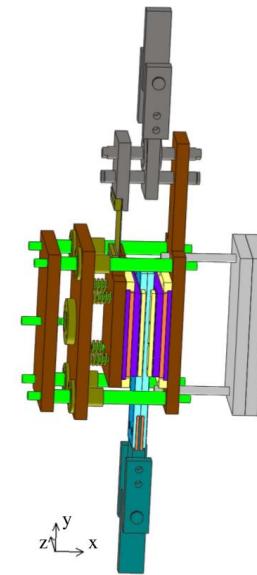
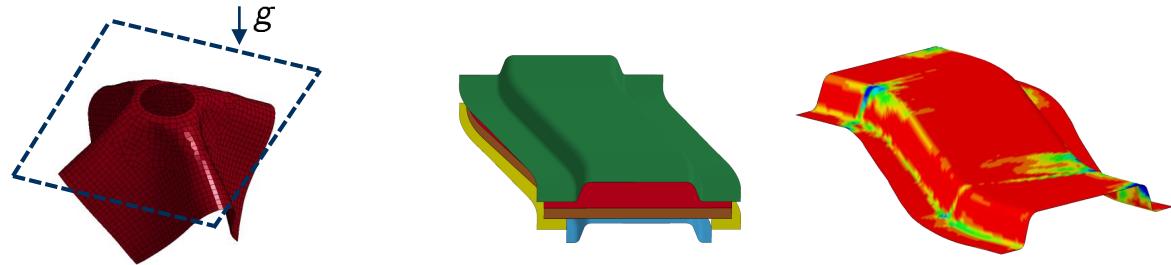
Summary

- ✓ Formulation for temperature dependent forming behavior of pre-consolidated fiber-reinforced thermoplastics
- ✓ Numerical modeling of thermoforming process



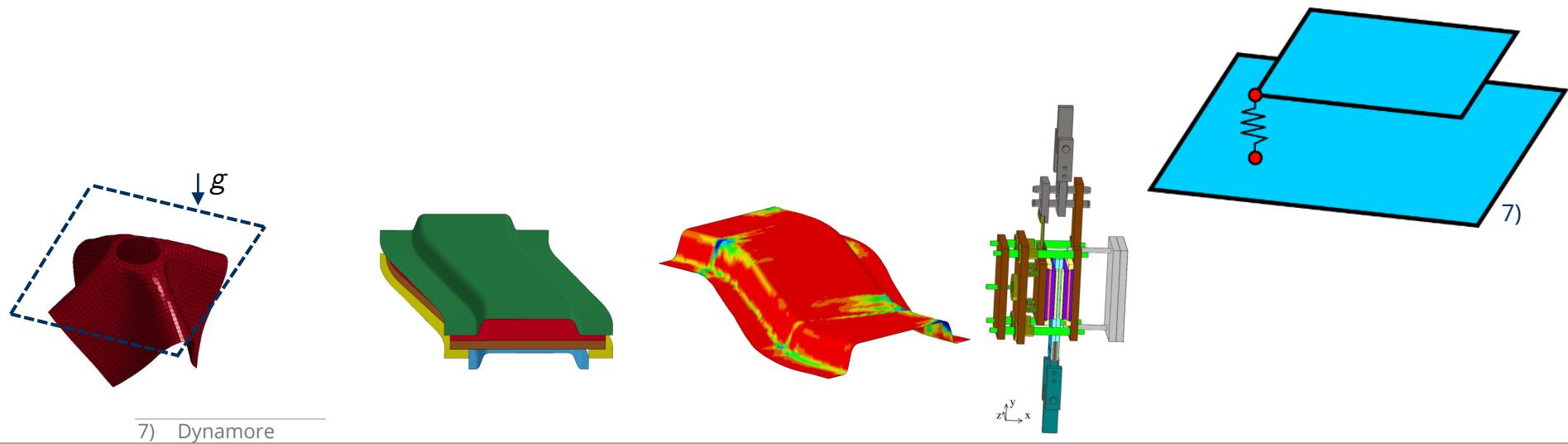
Summary

- ✓ Formulation for temperature dependent forming behavior of pre-consolidated fiber-reinforced thermoplastics
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Summary

- ✓ Formulation for temperature dependent forming behavior of pre-consolidated fiber-reinforced thermoplastics
 - ✓ Numerical modeling of thermoforming process
-
- Validation of material model (FRP) and determination of additional parameters
 - Considering of delamination



7) Dynamore

Summary

- ✓ Formulation for temperature dependent forming behavior of pre-consolidated fiber-reinforced thermoplastics
- ✓ Numerical modeling of thermoforming process
 - Validation of material model (FRP) and determination of additional parameters
 - Considering of delamination
 - Parameter studies of thermoforming

