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# CHARACTERIZATION OF A POLYURETHANE ADHESIVE AND COMPARATIVE CALIBRATION OF DIFFERENT MATERIAL MODELS IN LS-DYNA

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# Characterization and modelling of PU-adhesive

## Agenda

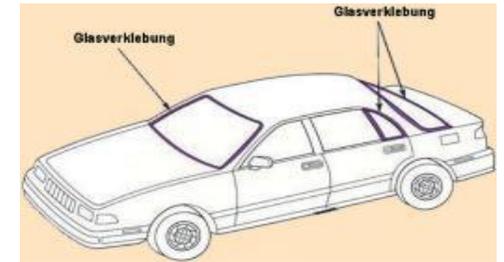
- **Background info**
  - PU-adhesive basic data
- **Characterization experiments**
  - tests with steel sheet adherends
  - tests with thick adherends and adhesive bulk substance
  - tests with bulk specimens
- **Simulation**
  - cohesive zone modelling with \*MAT-ARUP-ADHESIVE
  - elasto-plastic modelling with \*MAT-TAPO
  - user-defined hyperelastic material model from IfM Kassel
- **Résumé and future perspective**

# Characterization and modelling of PU-adhesive

## PU-adhesive basic data

- Polyurethane adhesive for semi-structural bonding in automotive industry [from technical data sheet of manufacturer]
  - single component adhesive
  - very good adhesion, also after overburning, on electro coatings and OEM clearcoats
  - shear modulus > 8 MPa
  - lap shear strength (after 7 days, 23 °C / 50 % r.h.) > 8 MPa
  - elongation at break > 300 %
- application of PU-adhesives for light-weight multi-material structures, e.g. bonding of wind shields
  - ability to withstand large elastic deformations, including deformation mismatching of structural parts
  - typical layer thicknesses of 3-6 mm

→ exploitation of stiffness and strength potential  
→ need for adequate modelling methods



Quelle: Chem. Unserer Zeit, 2008, 42, 92-101

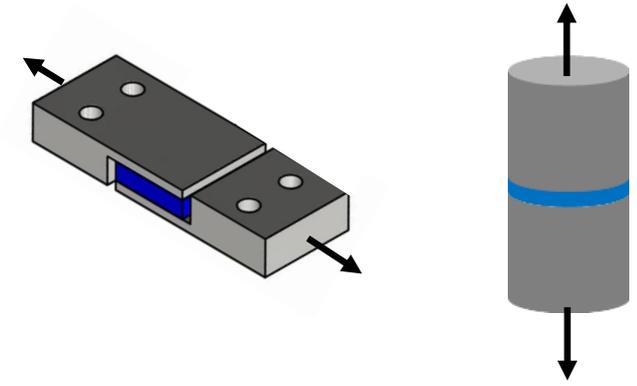
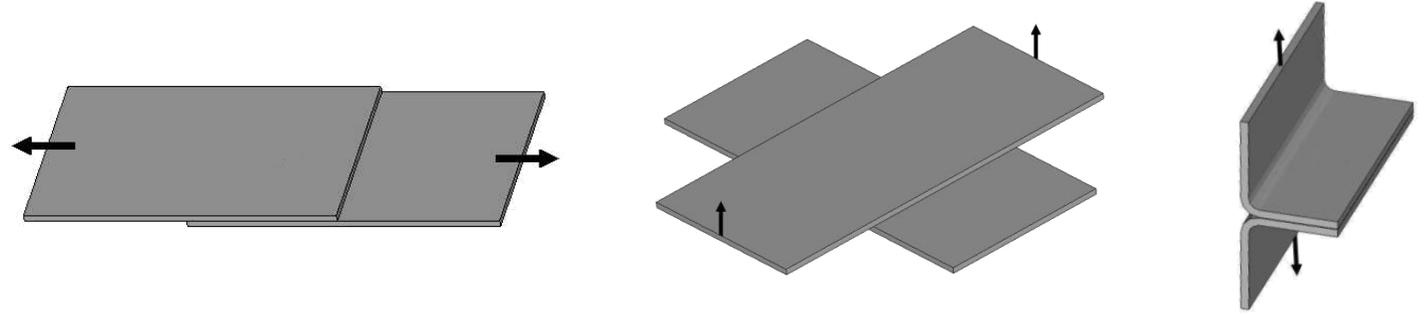


Quelle: MAN

# Characterization and modelling of PU-adhesive

## Experimental characterization

- **steel sheet adherends**  
quasi-static loading
  - single lap shear, cross tension, peel
- **thick steel adherends**  
different loading speeds
  - thick adherend shear, butt-joint tension (full circular bond area)
- **adhesive substance flat tension**  
quasi-static loading



# Characterization and modelling of PU-adhesive

## Experimental characterization – shear

### ■ Comparison of different experimental tests in shear loading single lap shear, quasi-static loading

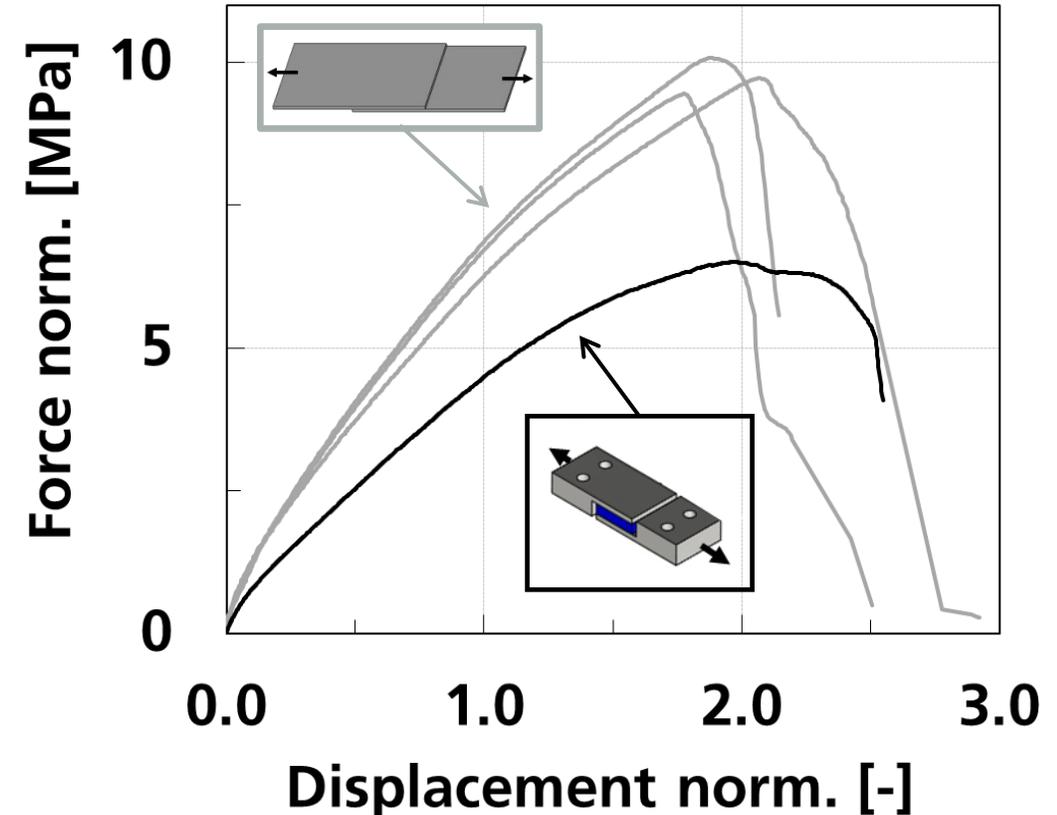
- steel sheet adherends ( $t_{\text{steel}} = 1.5 \text{ mm}$ ),  
 $t_{\text{adh}} = 3.6 \text{ mm}$ ,  $A_{\text{adh}} = 16 \times 45 \text{ mm}^2$



- “thick” steel adherends ( $t_{\text{steel}} = 1.5 \text{ mm}$ ),  
 $t_{\text{adh}} = 5 \text{ mm}$ ,  $A_{\text{adh}} = 16 \times 20 \text{ mm}^2$



- all tests show cohesive failure
- plastic deformation of steel adherends in both test types
- significantly higher normalized forces in steel sheet shear test
- strong influence of geometry (and possibly process parameters)

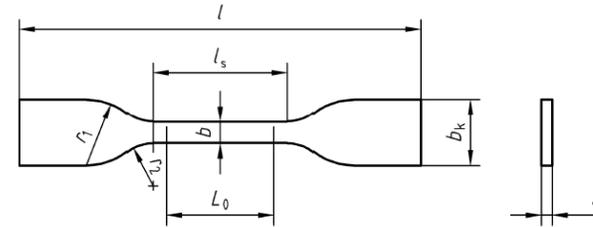


all diagrams: force normalized by adhesive bond area,  
displacement normalized by adhesive thickness

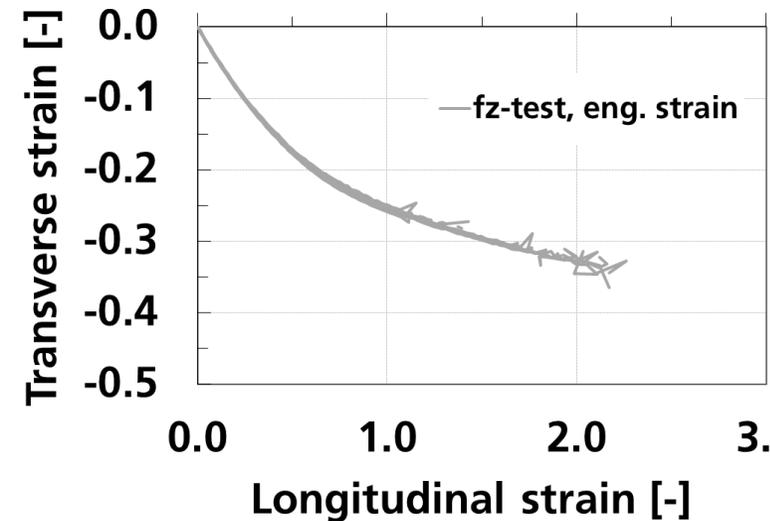
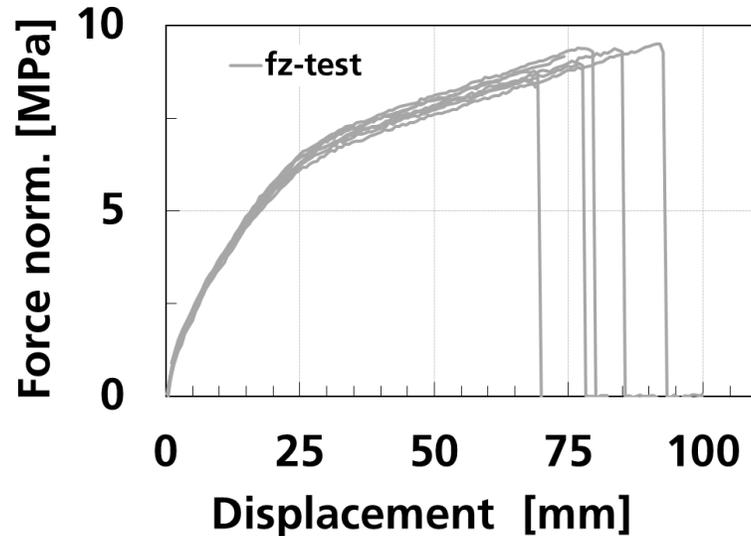
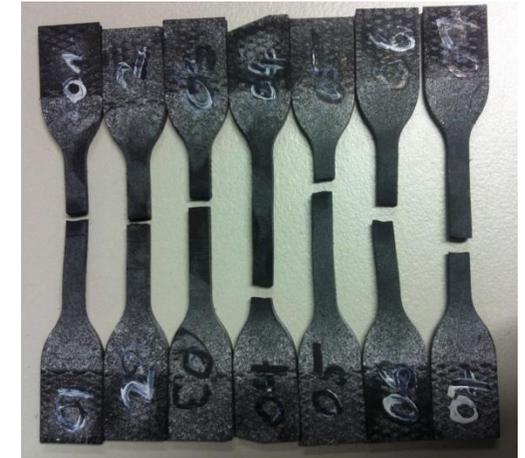
# Characterization and modelling of PU-adhesive

## Experimental characterization – substance flat tension

- adhesive substance flat tension test
  - quasi-static loading, Aramis strain measurement
  - elastic modulus ca. 22 MPa
  - nearly incompressible
  - more than 200 % elongation before fracture



$L_0 = 20 \text{ mm}$ ,  $L_s = 28 \text{ mm}$ ,  $b = 4 \text{ mm}$ ,  $a = 2.2 \text{ mm}$ ,  
(free deformation length = 45 mm,  $L_{0,\text{transv}} = 3 \text{ mm}$ )

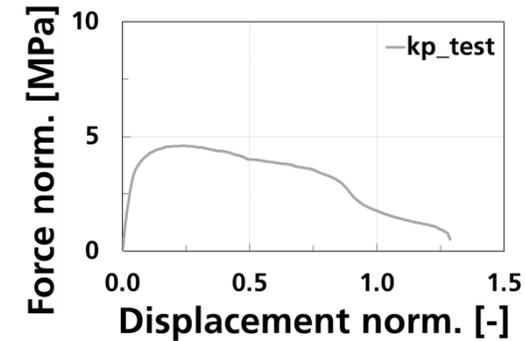


# Characterization and modelling of PU-adhesive

## Experimental characterization – tension with lateral constraint and peel

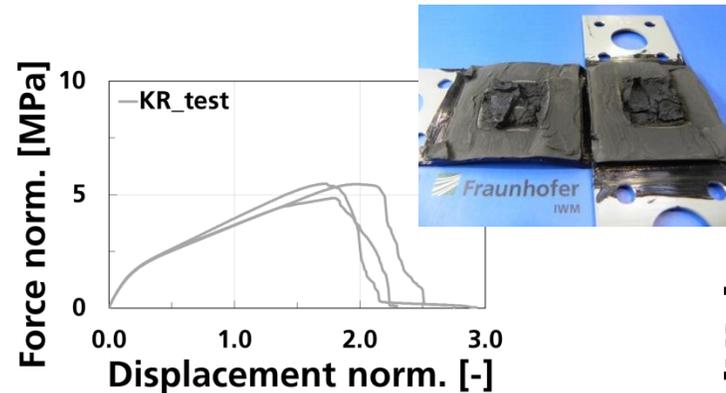
- butt-joint tension with steel adherend  
quasi-static loading, full circular bonding area

- $t_{adh} = 4 \text{ mm}$ ,  $\varnothing 20 \text{ mm}$



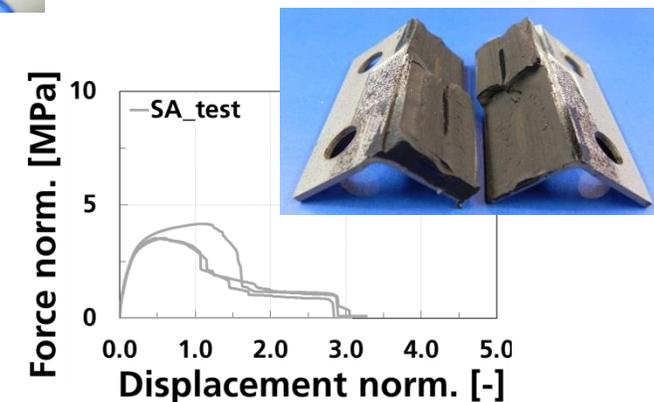
- cross tension with steel sheet adherend  
quasi-static loading

- adhesive:  $b \cdot l \cdot t_{adh} = 50 \cdot 50 \cdot 4 \text{ mm}^3$   
steel sheet:  $t = 1.5 \text{ mm}$



- peel test with steel sheet adherend  
quasi-static loading

- adhesive:  $b \cdot l \cdot t_{adh} = 50 \cdot 18 \cdot 4 \text{ mm}^3$   
steel sheet:  $t = 1.5 \text{ mm}$



all diagrams: force normalized by adhesive bond area,  
displacement normalized by adhesive thickness

# Characterization and modelling of PU-adhesive

## Modelling – cohesive zone model

### ■ \*MAT\_ARUP\_ADHESIVE (\*MAT\_169) (from LS-DYNA handbook)

- traction-separation laws for shear and tension
- elastic stiffness affected by initial thickness ( $L_0$ )  
stiffness modulus  $E'$  in tension  
(deformation constraint by stiff adherends)

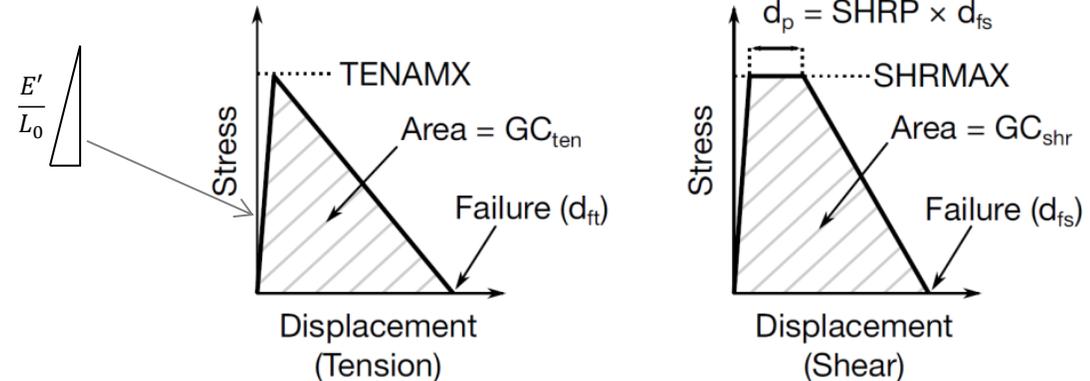
$$E' = \frac{E(1-\nu)}{(1-2\nu)(1+\nu)}$$

- yield and failure surfaces are treated as a power-law combination of direct tension and shear across the bond

$$\left(\frac{\sigma}{\sigma_{\max}}\right)^{\text{PWRT}} + \left(\frac{\tau}{\tau_{\max} - \text{SHT\_SL} \times \sigma}\right)^{\text{PWRS}} = 1.0$$

- parameter calibration:

- input: elastic modulus  $E$  and poisson ratio  $\nu$
- TENMAX / SHRMAX define yield stress
- GCTEN / GCSHR and SHRP define damage behavior and failure



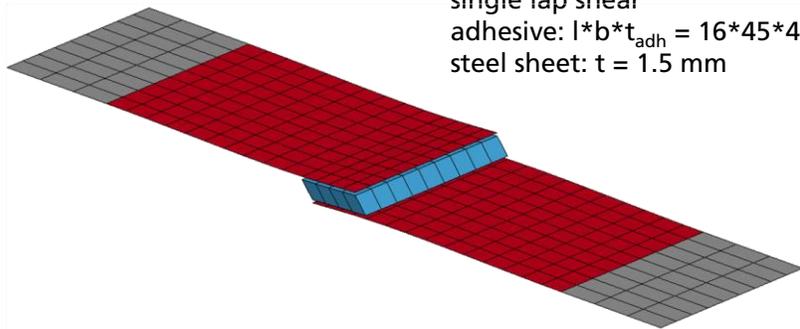
# Characterization and modelling of PU-adhesive

## Modelling – cohesive zone model

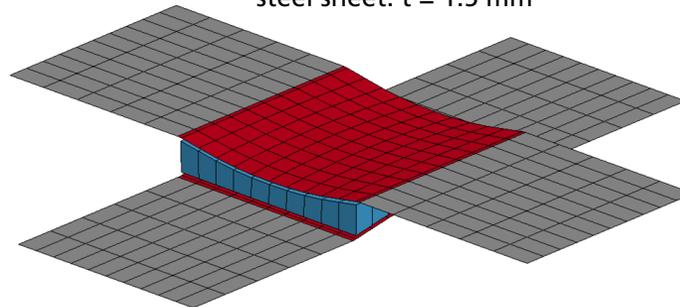
### ■ Mesh and modelling info

- adhesive (blue): \*MAT\_169, Elform=2,  $L_e$  ca. 5 mm / 1-2 mm
- steel sheet adherends: shells, Elform=16, red: \*MAT\_024 (calibrated elasto-plastic deformation behavior), grey: \*MAT\_rigid
- \*CONTACT\_TIED\_SHELL\_EDGE\_TO\_SURFACE\_CONSTRAINED\_OFFSET (Slave=part\_kleb, Master=part\_stahl)

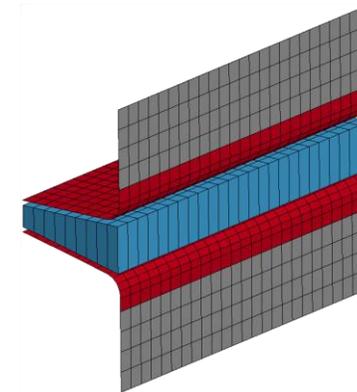
single lap shear  
adhesive:  $l*b*t_{adh} = 16*45*4 \text{ mm}^3$   
steel sheet:  $t = 1.5 \text{ mm}$



cross tension  
adhesive:  $b*l*t_{adh} = 50*50*4 \text{ mm}^3$   
steel sheet:  $t = 1.5 \text{ mm}$



peel  
adhesive:  $b*l*t_{adh} = 50*18*4 \text{ mm}^3$   
steel sheet:  $t = 1.5 \text{ mm}$



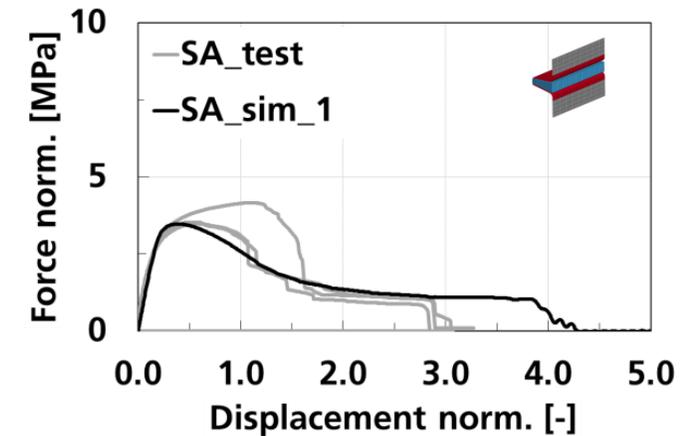
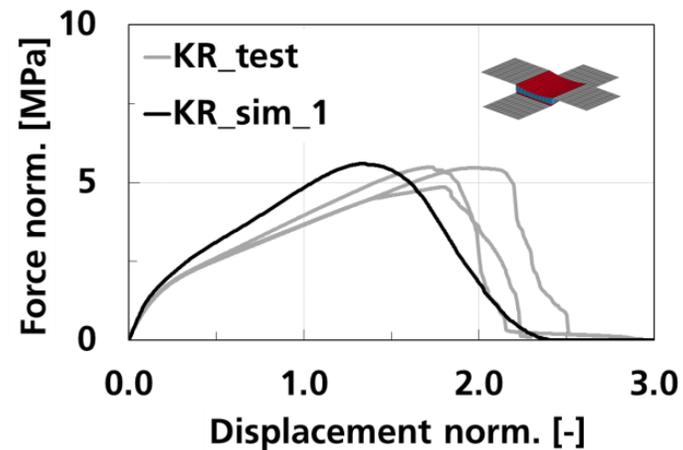
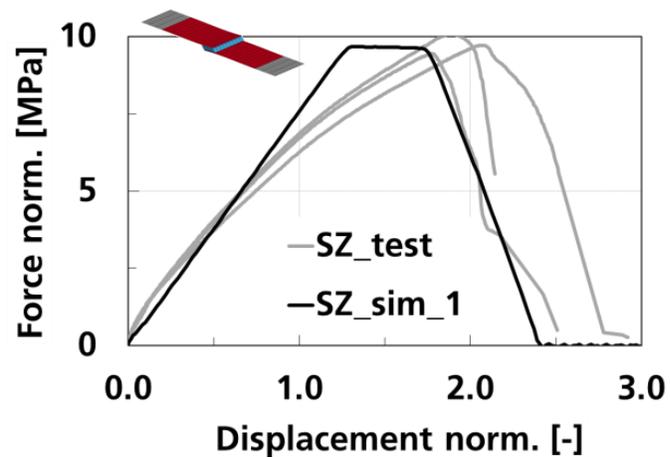
# Characterization and modelling of PU-adhesive

## Modelling – cohesive zone model

- Comparison of experimental results with simulation from different parameter sets

— experimental results

— calibration with sheet adherend specimens (parameter set 1)



all diagrams: force normalized by adhesive bond area, displacement normalized by adhesive thickness

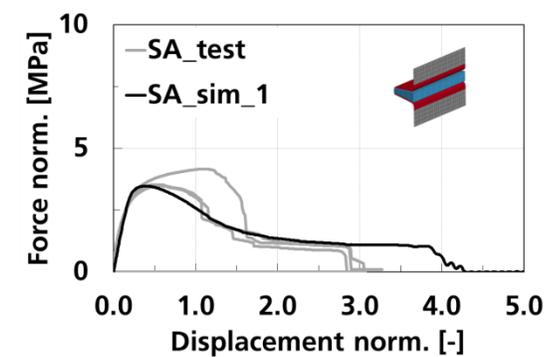
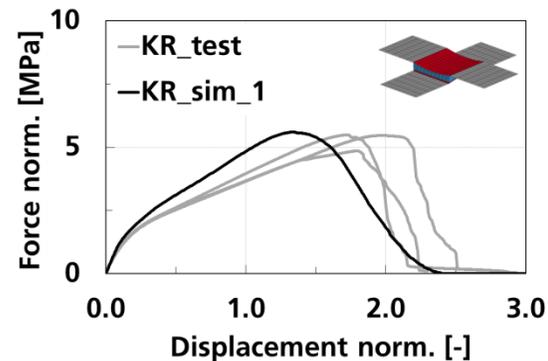
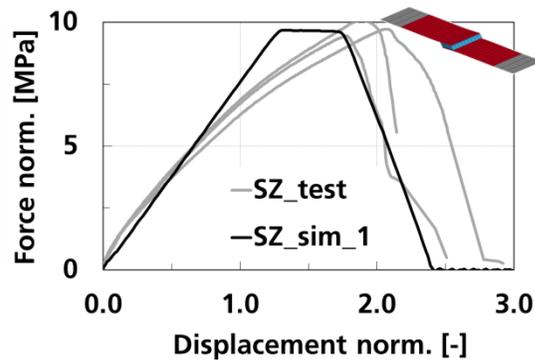
# Characterization and modelling of PU-adhesive

## Modelling – cohesive zone model

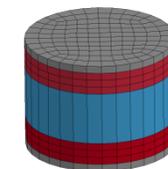
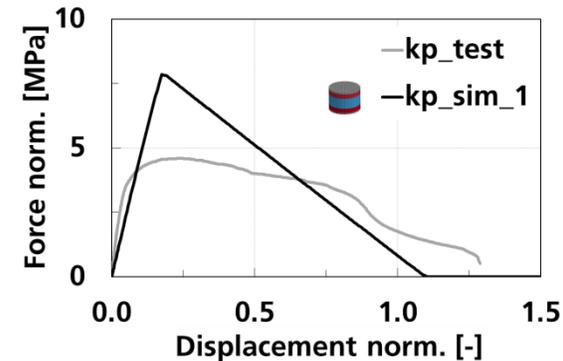
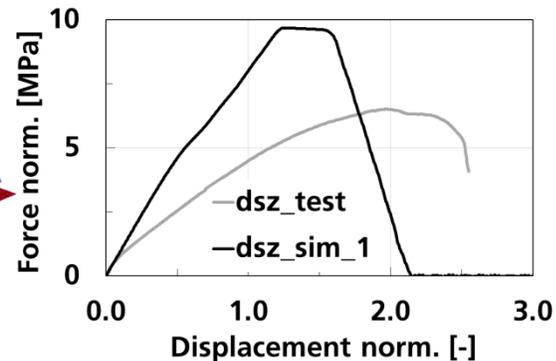
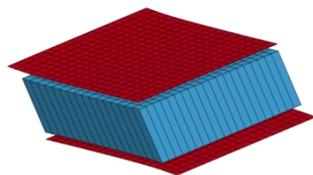
### ■ Comparison of experimental results with simulation from different parameter sets

— experimental results

— calibration with sheet adherend specimens (parameter set 1)



thick adherend  
shear  
adhesive:  
 $l \cdot b \cdot t_{adh} = 16 \cdot 20 \cdot 5 \text{ mm}^3$   
steel (in bond  
region):  
 $t = 1.5 \text{ mm}$



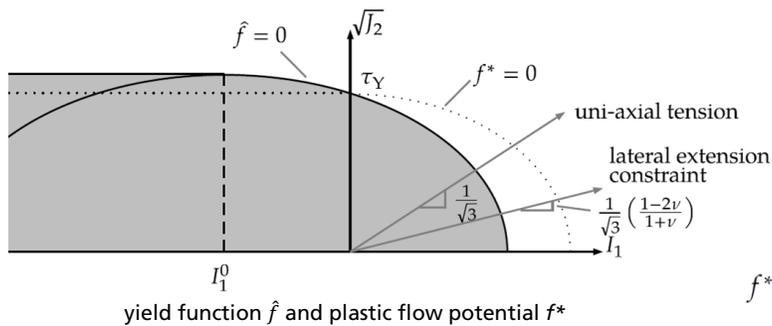
butt-joint tension  
 $r = 10 \text{ mm}$ ,  
adhesive:  
 $t_{adh} = 4 \text{ mm}$

all diagrams: force normalized by adhesive bond area, displacement normalized by adhesive thickness

# Characterization and modelling of PU-adhesive

## Modelling – 3D elasto-plastic material model

- **\*MAT\_TOUGHENED\_ADHESIVE\_POLYMER (TAPO, \*MAT\_252)**  
(from LS-Dyna handbook & Burbulla et al., 10<sup>th</sup> European LS-Dyna Conference, 2015)
  - non-associated, elasto-viscoplastic material model for crash optimized high-strength adhesives under combined shear and tensile loading
  - (rate-dependent) yield strength  $\tau_Y$  with non-linear hardening contribution  $R$   $\tau_Y = (\tau_0 + R) \quad R = q[1 - \exp(-br)] + Hr$
  - softening due to damage, rate-dependency, and constitutive description for mechanical behavior under compression



$$\hat{f} := \frac{J_2}{(1-D)^2} + \frac{a_2}{3} \left\langle \frac{I_1}{1-D} + \frac{\sqrt{3}a_1\tau_0}{2a_2} \right\rangle^2 - \left( \tau_Y^2 + \frac{a_1^2\tau_0^2}{4a_2} \right) = 0$$

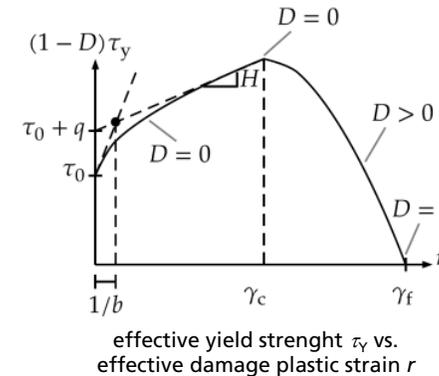
yield function  $\hat{f}$  with first invariant of the stress tensor  $I_1$  and second invariant of the stress deviator  $J_2$

$$I_1 = \text{tr } \sigma \quad J_2 = (1/2)\text{tr}(\mathbf{s})^2$$

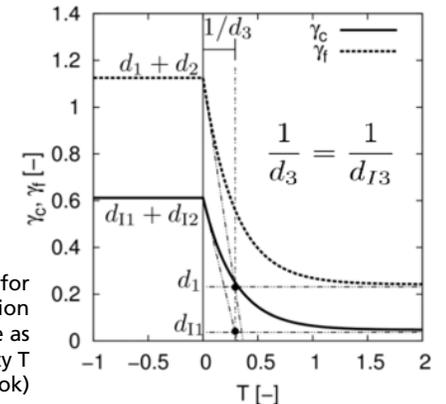
$$f^* := \frac{J_2}{(1-D)^2} + \frac{a_2^*}{3} \left\langle \frac{I_1}{1-D} \right\rangle^2 - \tau_Y^2 \quad a_2^* = \frac{1-2\nu^*}{2(1+\nu^*)}$$

plastic potential  $f^*$  with parameter  $a_2^*$  to influence plastic dilatation, to be identified from uni-axial tension test

$$\nu^* = -\frac{\epsilon_{\text{trans}}^{\text{pl}}}{\epsilon_{\text{axial}}^{\text{pl}}}$$



threshold strains for damage initiation and rupture as function of triaxiality  $T$  (Johnson & Cook)



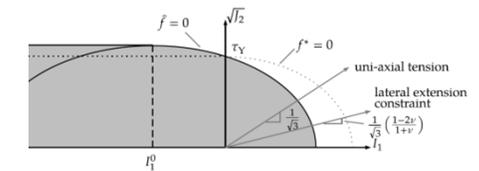
# Characterization and modelling of PU-adhesive

## Modelling – 3D elasto-plastic material model

### ■ \*MAT-TAPO parameter calibration for deformation behavior

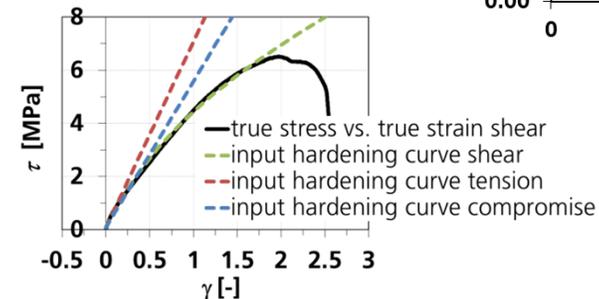
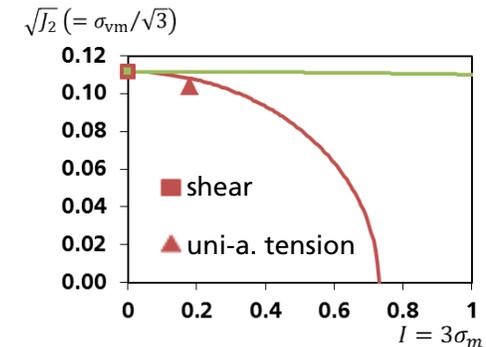
#### ■ elliptical yield function form directly from experimental results: yield stress in shear loading and uni-axial tensile loading

- no additional data from compression or mixed-mode shear-tension tests available →  $I_1^0 = 0$  ( $a_{10} = 0$ )
- *difficulty*: large elastic deformation capacity of the PU adhesive → low ratio of elastic modulus to material strength → instability problems → unrealistic high elastic modulus & low yield stress levels



#### ■ input $E = 1000$ MPa, $\nu = 0.49$ (→ $G = 335$ MPa) yield function ellipse with $\tau_0 = 0.1116$ MPa (shear) and $\sigma_0 = 0.15$ MPa (uni-a. tension)

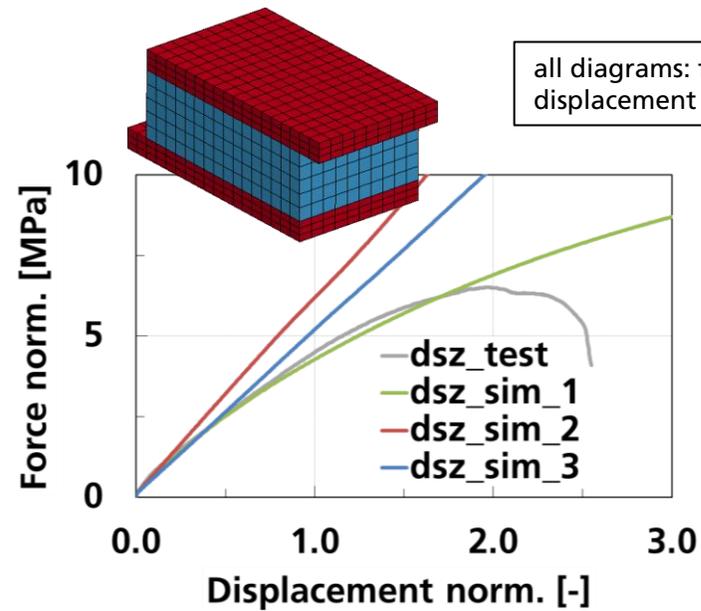
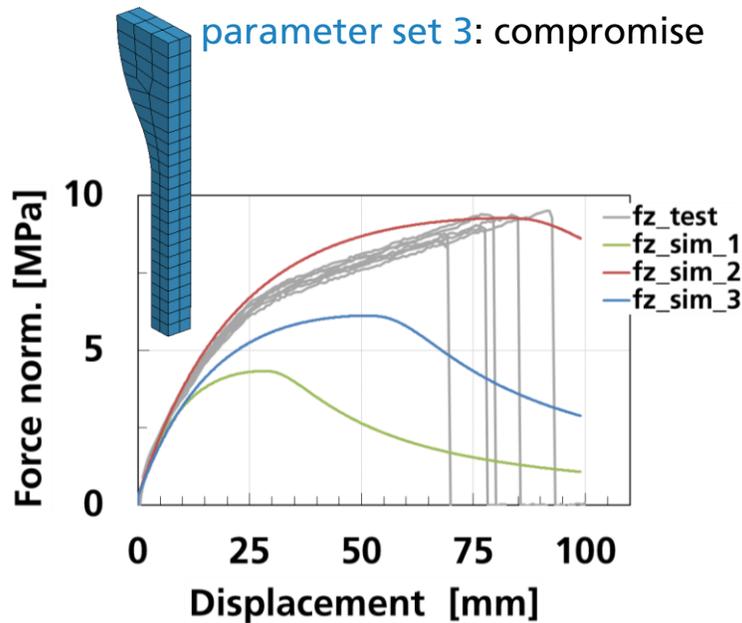
- *difficulty*: very flat ellipse shape (green line) needed to reproduce deformation behavior in butt-joint tension test → this results in early localization in uni-axial tension
- *difficulty*: hardening behavior from shear test does not fit deformation behavior in uni-axial tensile loading → compromise hardening input
- → either uni-axial tension or shear and constrained tension deformation can be reproduced



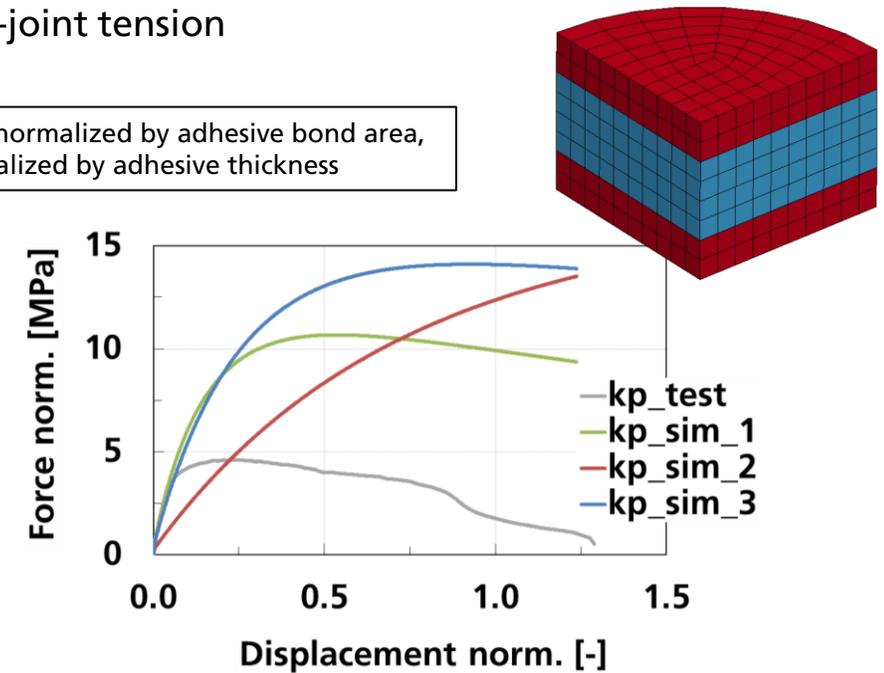
# Characterization and modelling of PU-adhesive

## Modelling – 3D elasto-plastic material model

- \*MAT-TAPO parameter calibration for deformation behavior
  - adhesive (blue): \*MAT\_252, Elform=1,  $L_e = 1$  mm; steel adherends (red): \*MAT\_024, Elform=2
  - parameter set 1: to reproduce shear and butt-joint tension → trade-off for uni-axial tension
  - parameter set 2: to reproduce uni-axial tension → trade-off for shear and butt-joint tension
  - parameter set 3: compromise



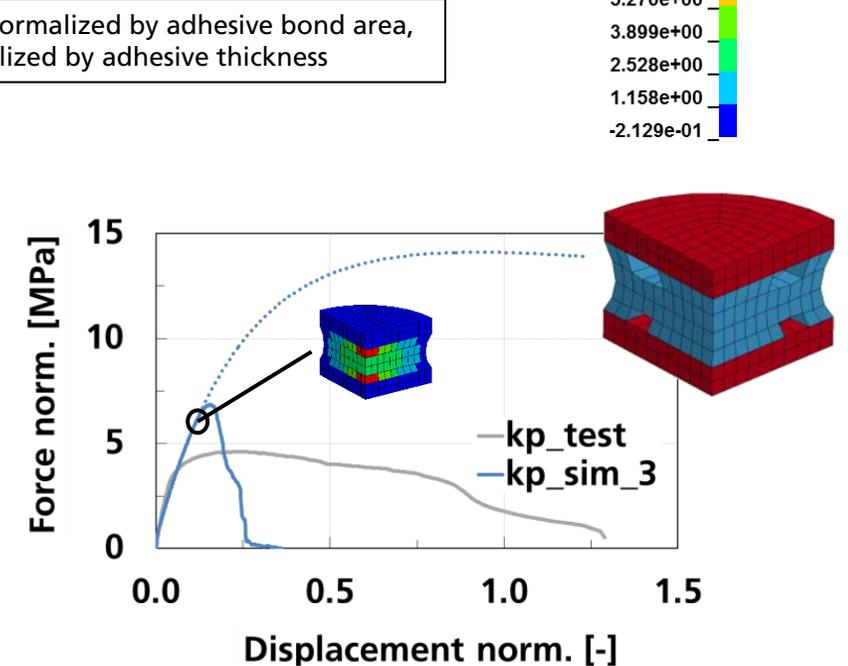
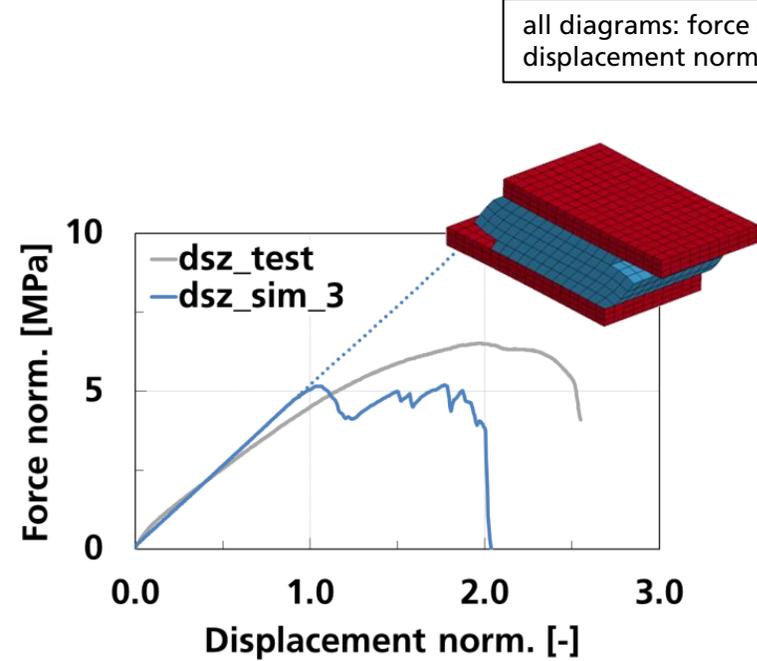
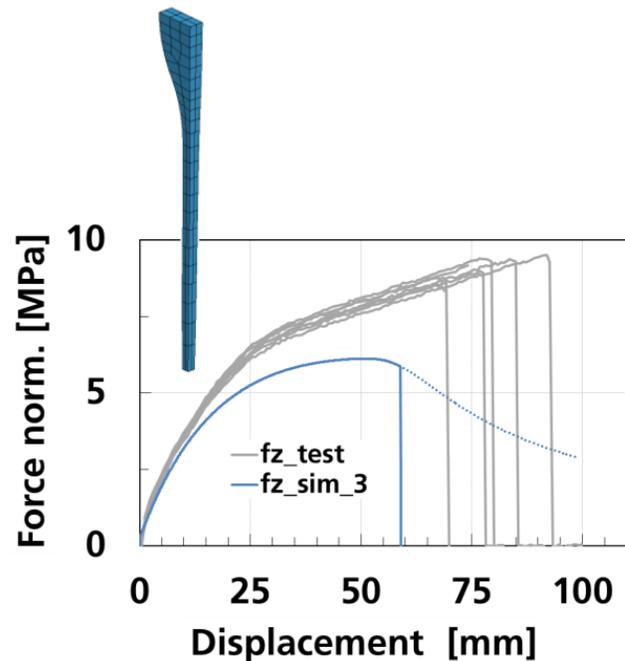
all diagrams: force normalized by adhesive bond area,  
displacement normalized by adhesive thickness



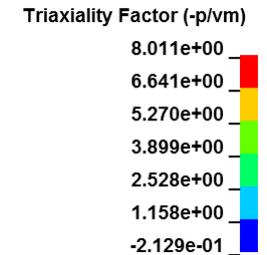
# Characterization and modelling of PU-adhesive

## Modelling – 3D elasto-plastic material model

- \*MAT-TAPO parameter calibration for failure behavior
  - paramter set 3: compromise in deformation behavior
  - damage initiation and failure curves



all diagrams: force normalized by adhesive bond area,  
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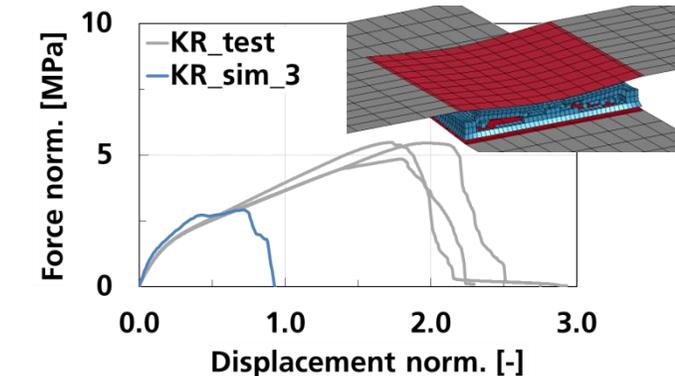
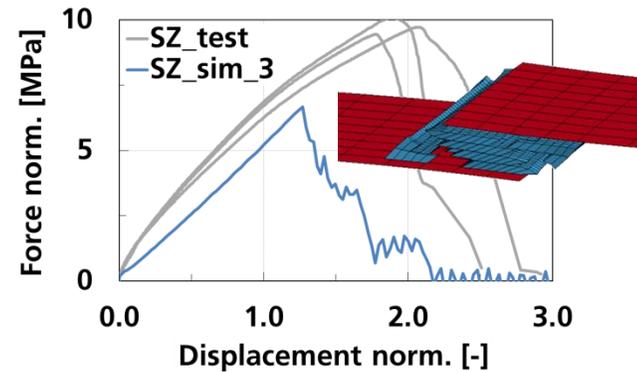
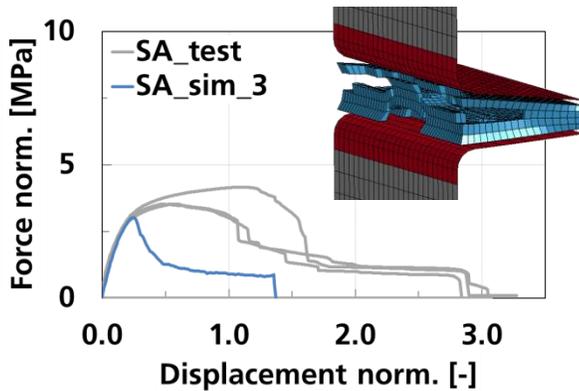
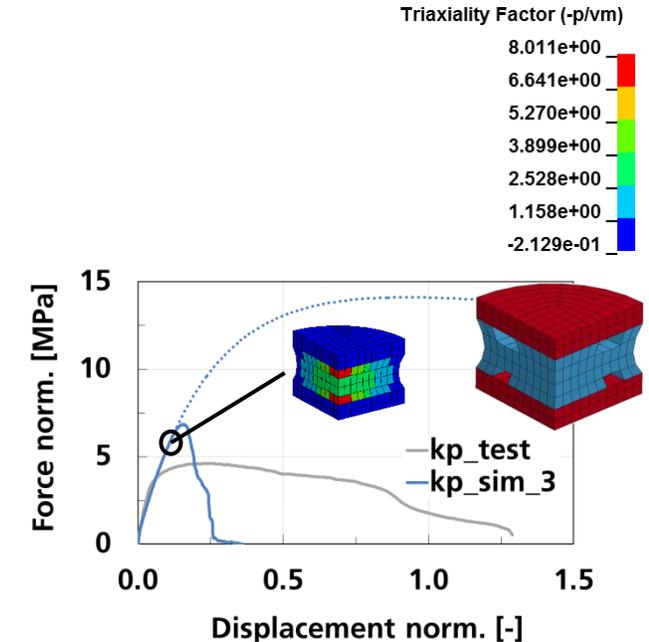
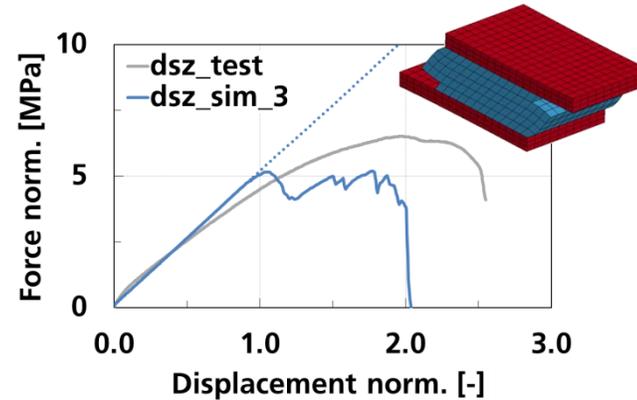
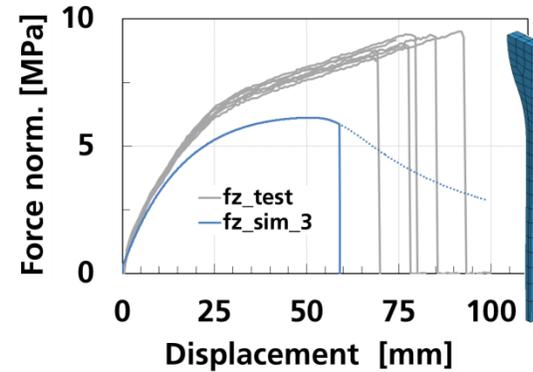


# Characterization and modelling of PU-adhesive

## Modelling – 3D elasto-plastic material model

- \*MAT-TAPO parameter calibration for failure behavior

- paramter set 3: compromise in deformation behavior
- damage initiation and failure curves



all diagrams: force normalized by adhesive bond area, displacement normalized by adhesive thickness

# Characterization and modelling of PU-adhesive

## Modelling – 3D hyperelastic material model

### ■ hyperelastic user-defined material model by IfM (\*)

■ deviatoric-volumetric split  $\bar{\mathbf{F}} = J^{-1/3} \mathbf{F}$   $J = \det(\mathbf{F}) = \sqrt{\det(\mathbf{C})}$   $\bar{\mathbf{B}} = \bar{\mathbf{F}} \cdot \bar{\mathbf{F}}^T = J^{-2/3} \mathbf{F} \cdot \mathbf{F}^T$

■ strain energy density function

$$W(\mathbf{B}) = \underbrace{\frac{1}{2}c_{10}(I_{\bar{\mathbf{B}}} - 3) + \frac{1}{2}c_{01}(II_{\bar{\mathbf{B}}} - 3)}_{W^{\text{iso}}} + \underbrace{K(J - 1 - \ln J)}_{W^{\text{vol}}}$$

MOONEY-RIVELIN model [from \*\*]

■ resulting stress-strain relationship

$$\mathbf{T} = \frac{1}{J} \left( (c_{10} + c_{01} I_{\bar{\mathbf{B}}}) \bar{\mathbf{B}}^D - c_{01} (\bar{\mathbf{B}}^2)^D \right) + \frac{1}{J} K (J - 1) \mathbf{1}$$

3 deformation parameters

■ continuum damage mechanics  
energy based failure model

$$D^{\text{iso}} = \left\langle \frac{W^{\text{iso}}(I_{\bar{\mathbf{B}}}, II_{\bar{\mathbf{B}}}) - W_{\text{fl}}^{\text{iso}}}{W_{\text{fc}}^{\text{iso}} - W_{\text{fl}}^{\text{iso}}} \right\rangle \quad D^{\text{vol}} = \left\langle \frac{W^{\text{vol}}(J) - W_{\text{fl}}^{\text{vol}}}{W_{\text{fc}}^{\text{vol}} - W_{\text{fl}}^{\text{vol}}} \right\rangle \quad \mathbf{T} = (1 - D)(\mathbf{T}^{\text{iso}} + \mathbf{T}^{\text{vol}}) \quad D = \max[D^{\text{iso}}, D^{\text{vol}}]$$

3 damage initiation parameters,  
3 failure parameters

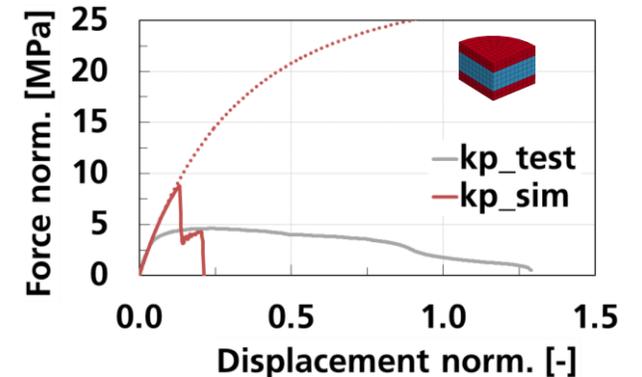
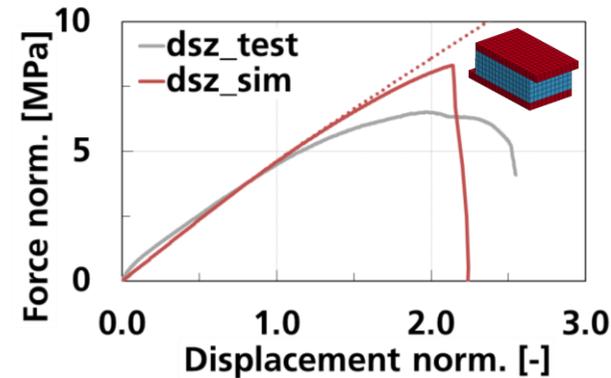
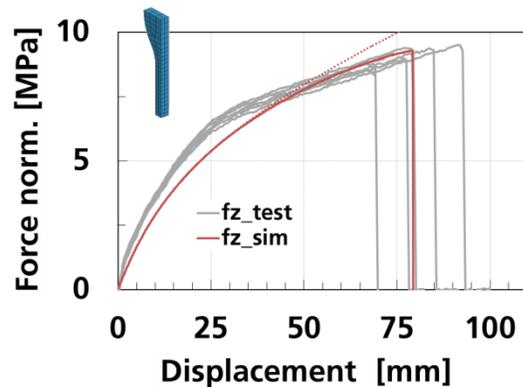
\* Nelson, A., Matzenmiller, „Modelling and finite element analysis of cavitation and isochoric failure of hypereleastic adhesives“, proc.10th Conf. on Constitutive Models for Rubber (ECCMR X), 357-363, 2017.

\*\* Miehe, C., „Computation of isotropic tensor functions“, Communications in Numerical Methods in Engineering, 9:889-896, 1993.

# Characterization and modelling of PU-adhesive

## Modelling – 3D hyperelastic material model

- hyperelastic user-defined material model by ifm
  - parameter calibration for deformation and failure behavior



all diagrams: force normalized by adhesive bond area, displacement normalized by adhesive thickness

# Characterization and modelling of PU-adhesive

## Résumé

- **experimental characterization**
  - similar loading conditions may lead to different results
    - shear strength from sheet adherend tests ca. 1.5 times higher than from „thick“ adherend tests
    - → strong influence of geometry, smaller specimens tend to have stronger influence of notch effects
    - influence of adhesive bonding process must be taken into account
- **material models**
  - cohesive zone modelling with \*MAT-ARUP
    - acceptable agreement with experimental results, simple calibration procedure, elastic deformation represented
  - MAT-TAPO
    - not suited for large elastic deformations, differences in deformation behavior in shear and tension are not covered, damage and failure behavior not very well represented especially in butt-joint loading
  - hyperelastic MAT-user-defined by IfM
    - deformation behavior well represented, including unloading; damage and failure behavior: different models still tested

# Characterization and modelling of PU-adhesive

## Future perspective

- parameter calibration based on DVC 3D-strain field analysis (joint Fraunhofer IWM & IMWS research project)
  - 3D strain field analysis of PU-adhesive layer for advanced material model calibration by CT-measurement and digital volume correlation (DVC) method

example of displacement vector analysis in shear test (different specimen)

