

# Neue Entwicklungen in LS-OPT/Topology - Ausblick auf Version 2

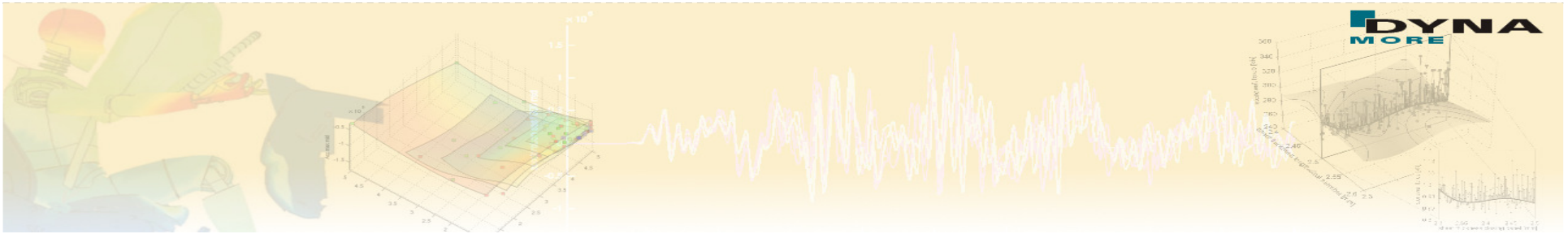
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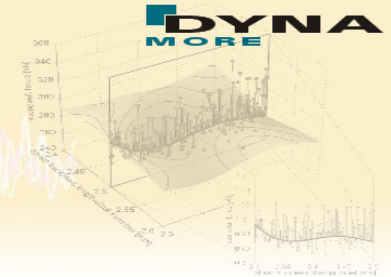


## → Overview

- Introduction
- Topology Optimization for Crash
  - *Equivalent Static Load Method*
  - *HCA Method - Implementation in LS-OPT/Topology*
- Application Example
- Conclusions

# Introduction

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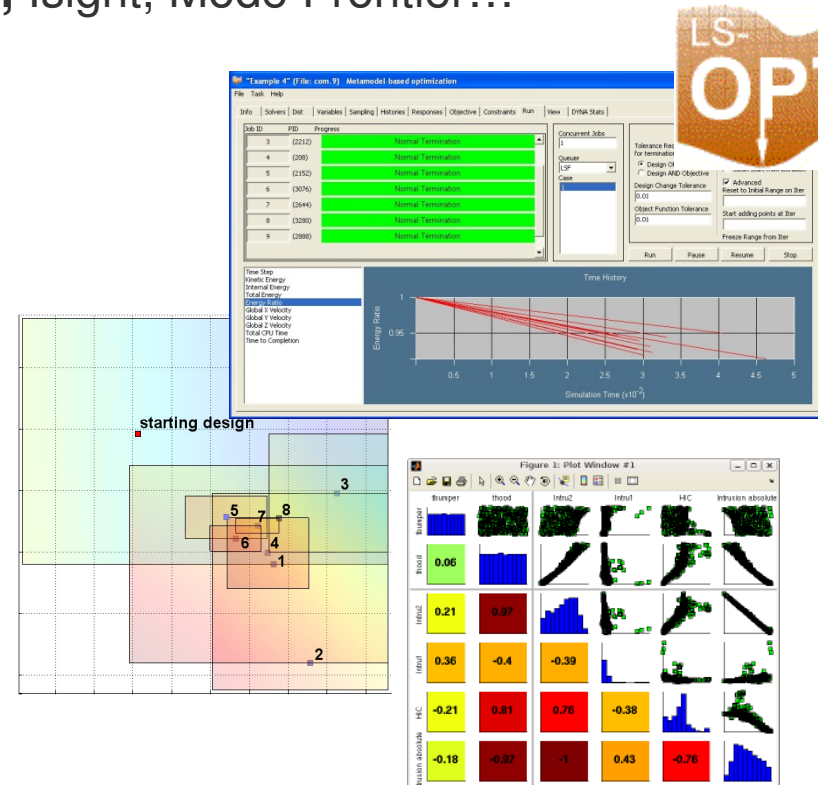
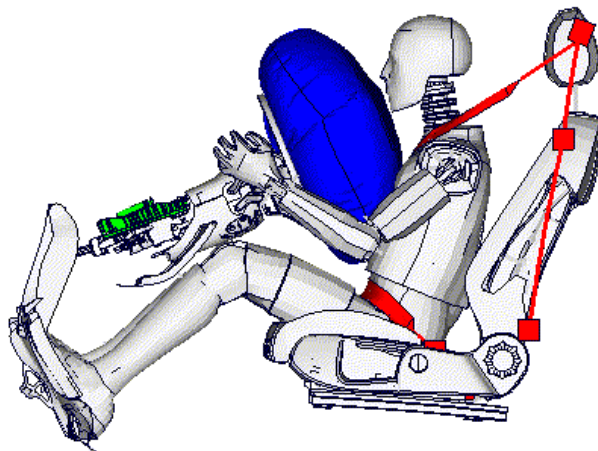


## ➔ Non-Linear Optimization

■ Available Software Products: **LS-OPT**, Isight, Mode Frontier...

### Non-linear / Parametric

- Parameterization of input files
- Shape/Sizing Optimization
- Possible for general nonlinear applications: Crash, Fluid Dynamics, Nonlinear Static/Dynamic



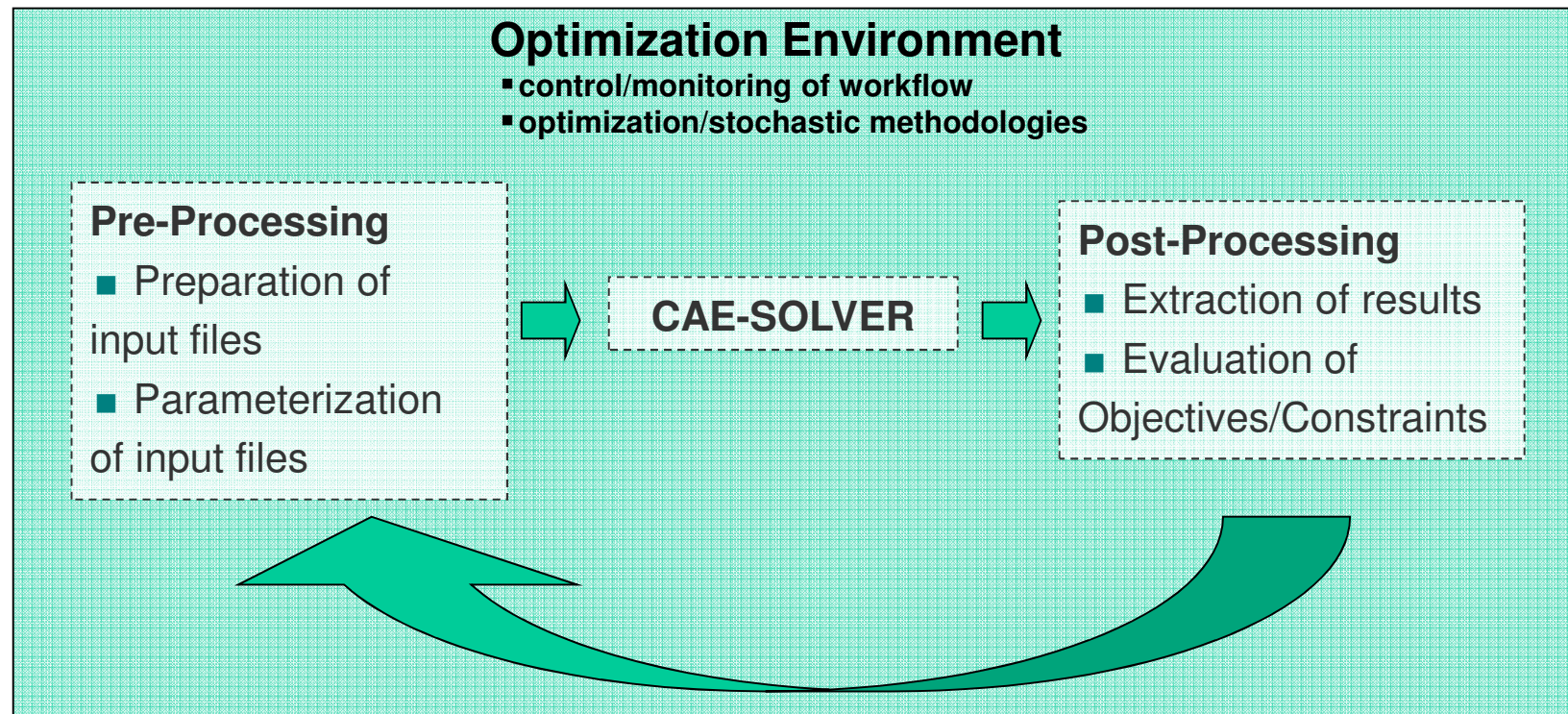
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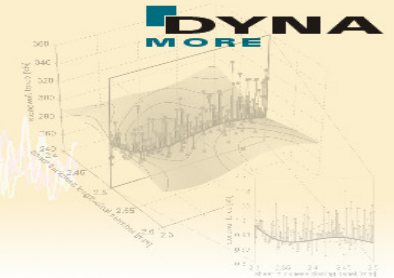
## ➔ Non-Linear Optimization

### ■ Process Flow for Parametric Optimization - Simplified Representation



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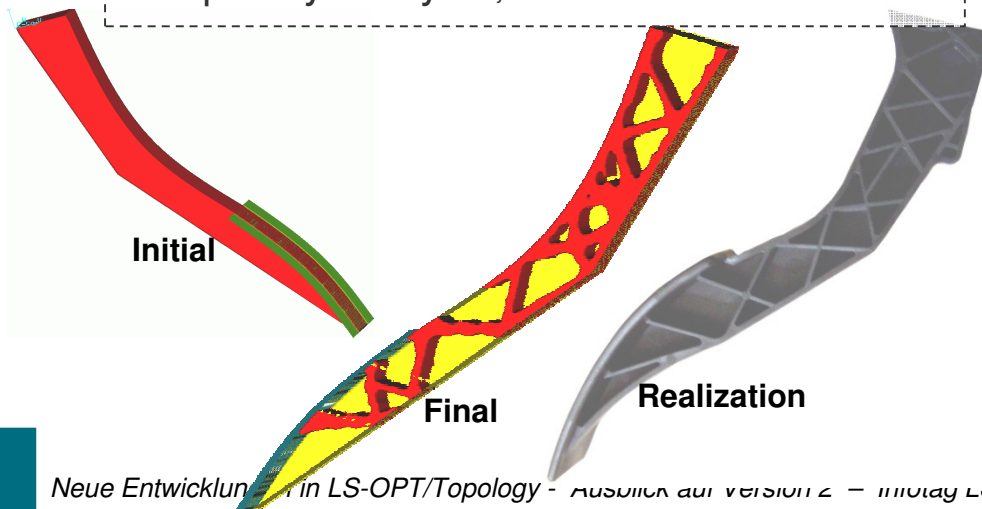
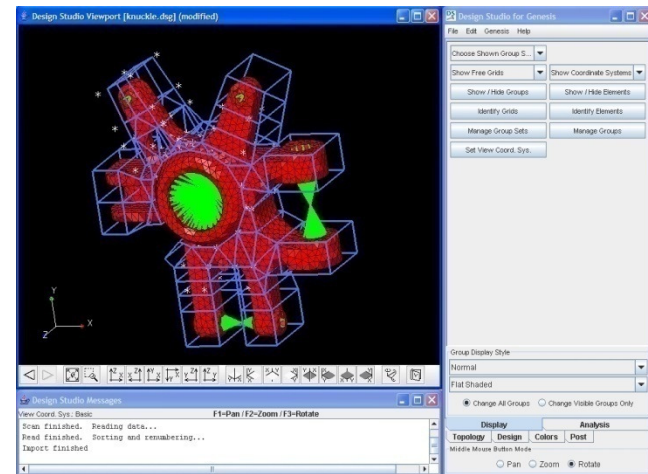
## ➔ Linear Optimization

■ Available Software Products: **Genesis**, Optistruct, Tosca...



### Non-Parametric

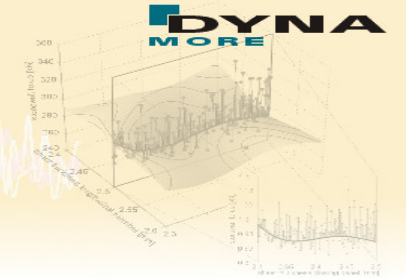
- Topology / Topometry Optimization
- Usually Linear FE-Problems
- Gradient based solvers – many design variables > 1000000
- CAE-Applications: Static Loads, Frequency Analysis, NVH





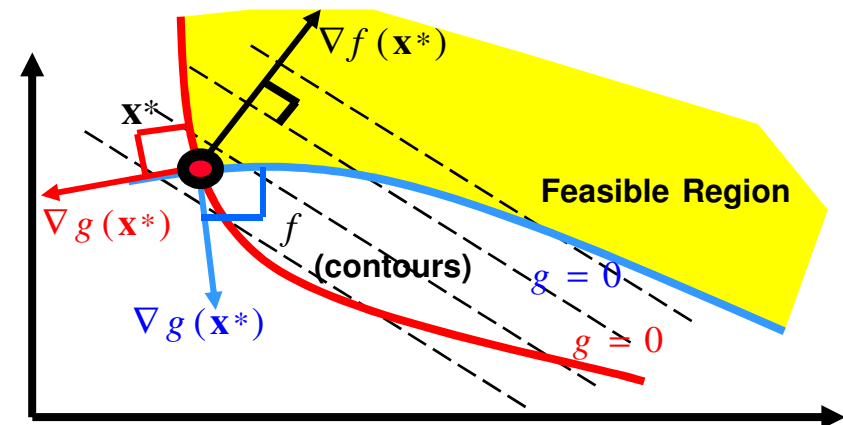
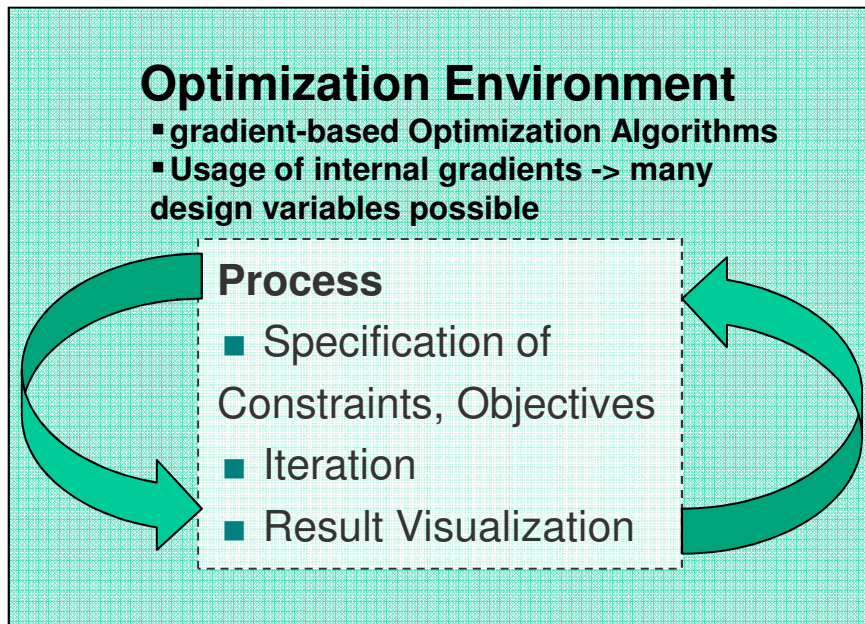
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## → Linear Optimization

- Usually Integrated FE-Solver



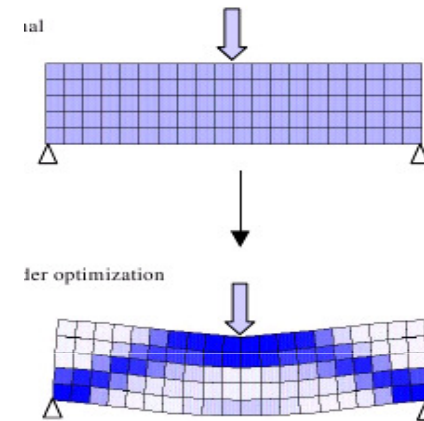
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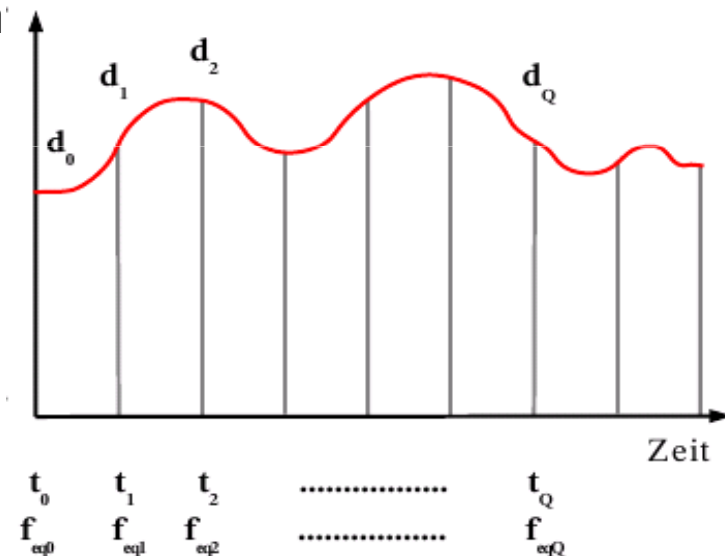
## → Topology Optimization for Crash

- For topology optimization each element is a design variable - can be switched on/off
  - many variables
    - *Can not be solved with LS-OPT (too many variables)*
    - *Can not be solved for crash with gradient based topology solvers like e.g. Genesis (strong non-linearities)*
- Two considerable approaches
  - *Equivalent Static Loads Method – ESLM*
  - *Hybrid Cellular Automata – HCA*



## → Equivalent Static Loads Method – ESLM

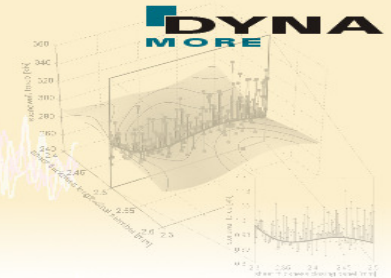
- An *Equivalent Load* is a load in a linear static system that makes an identical response to that in a nonlinear system
- Linear multi load case optimization for each time step  $t_i$  with equivalent static loads
- Has to be proven for large deformations such as buckling, folding
- Difficult to account for boundary conditions like reaction forces



### ■ References

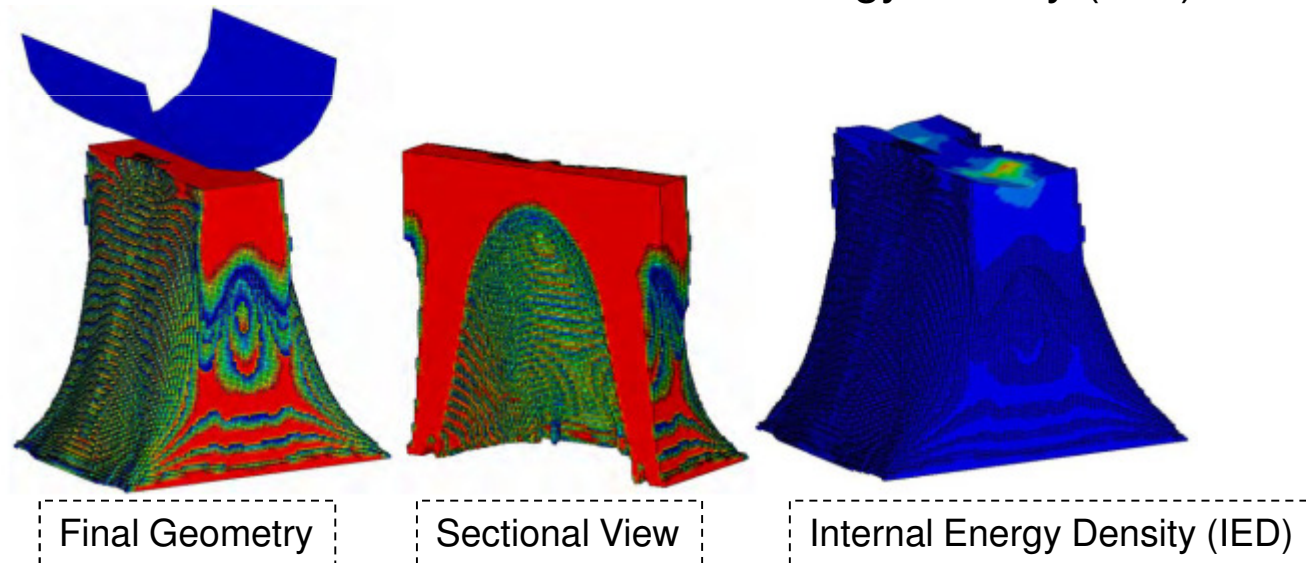
- M.K. Shin, K.J. Park, G.J. Park (2007), “Optimization of Structures with Nonlinear Behavior Using Equivalent Loads,” *Computer Methods in Applied Mechanics and Engineering*, Vol. 196, pp. 1154-1167
- Kosaka, I. (Vanderplaats R&D) “Improvement of Energy Absorption for the Side Member using Topography Optimization” *LS-DYNA World Conf.* 2010





## → Hybrid Cellular Automata – HCA

- Implemented in LS-OPT/Topology
- Gradient free, heuristic method
- Objective is to achieve a uniform internal energy density (IED) distribution

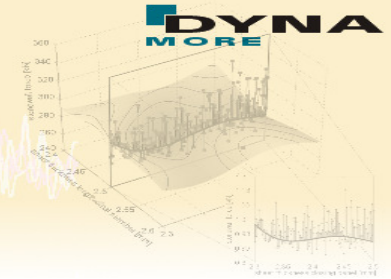


### ■ Reference

- T. Goel, W. Roux, N. Stander; “A topology optimization tool for LS-DYNA users: LS-OPT/Topology”  
7<sup>th</sup> European LS-DYNA Conference, Salzburg, 2009

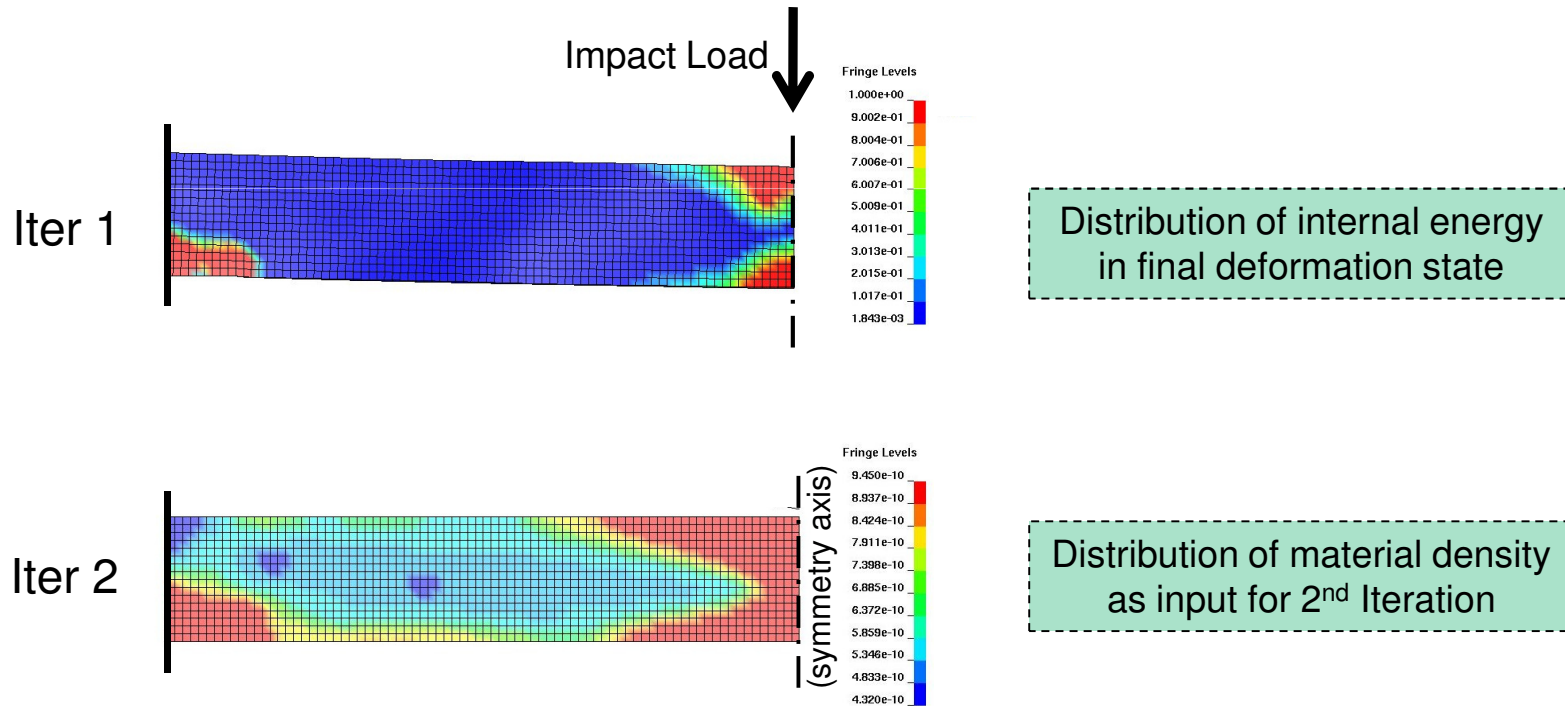
# Methods

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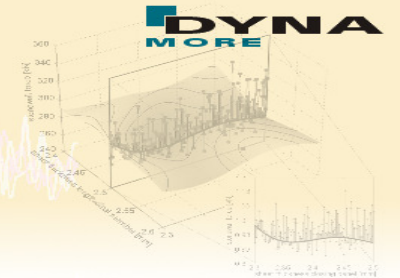
## → Hybrid Cellular Automata – HCA

- Demo Example of Method (beam, supported at both ends)



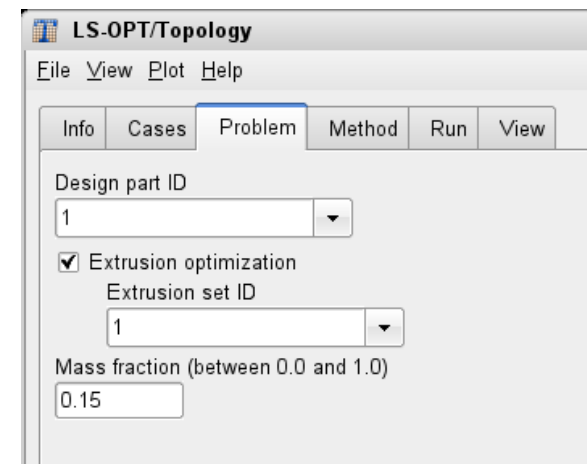
# Implementation

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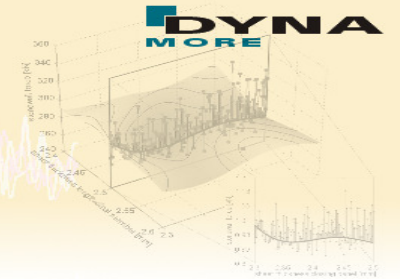
## → LS-OPT/Topology - Version V1.0

- Current Version is V1.0 – released end of 2009
- Download at <http://www.lsoptsupport.com/downloads>
- For now available settings within the LS-DYNA model
  - Element type: eight-noded solid elements
  - Material model: \*MAT\_PIECEWISE\_LINEAR\_PLASTICITY
  - Contact types: \*CONTACT\_AUTOMATIC\_SURFACE\_TO\_SURFACE and \*CONTACT\_AUTOMATIC\_SINGLE\_SURFACE
- Objective is fixed in obtaining uniform internal energy density in the structure
- For now two types of constraints are available:
  - Mass fraction
  - Extrusion



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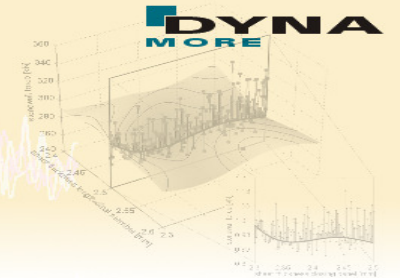
## → LS-OPT/Topology - Version V1.0

- Large models (1 million elements) can be handled
- Arbitrary-shaped domain can be designed
- Both linear and non-linear problems can be solved
- Can be readily hooked with queuing systems
- Evolves topology very quickly
- The tool can also work with multiple load cases (not demonstrated here)



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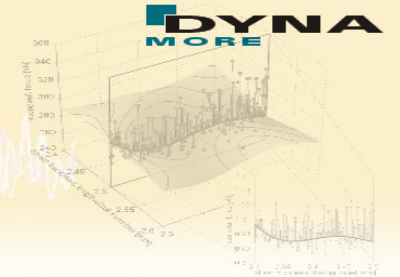


## → LS-OPT/Topology – Outlook Version 2

- Upcoming Version is V2.0 –
  - Alpha: On request.
  - Beta: December 2010
  - Release: March 2011
- Double the amount of code relative to version 1, so this may take some time to stabilize

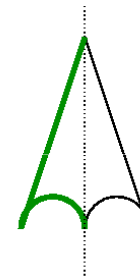
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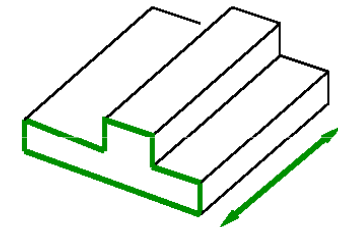


## → LS-OPT/Topology – Outlook Version 2

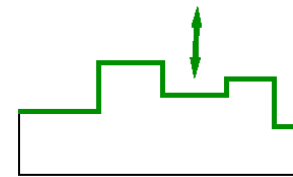
- Global Constraints e.g. maximum displacements
- Shell structures
- Multiple parts
- Symmetry constraint
- Casting direction constraint
- Tetrahedral elements



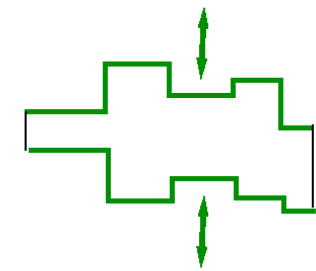
Symmetry



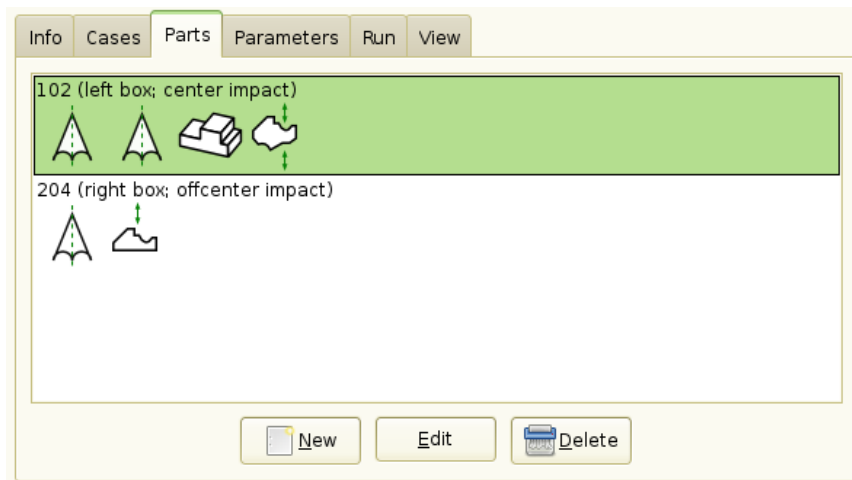
Extrusion



One-sided Casting

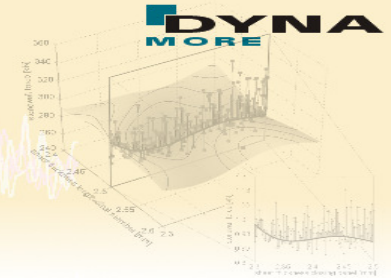


Two-sided Casting



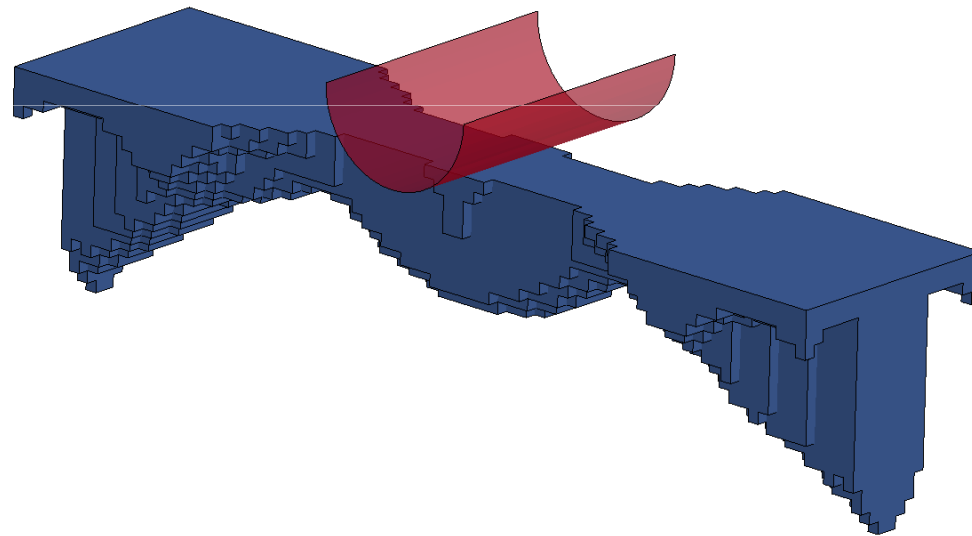
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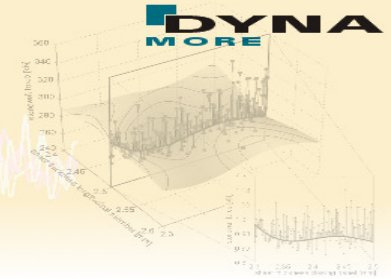
## → LS-OPT/Topology – Outlook Version 2

- Examples Casting Constraints



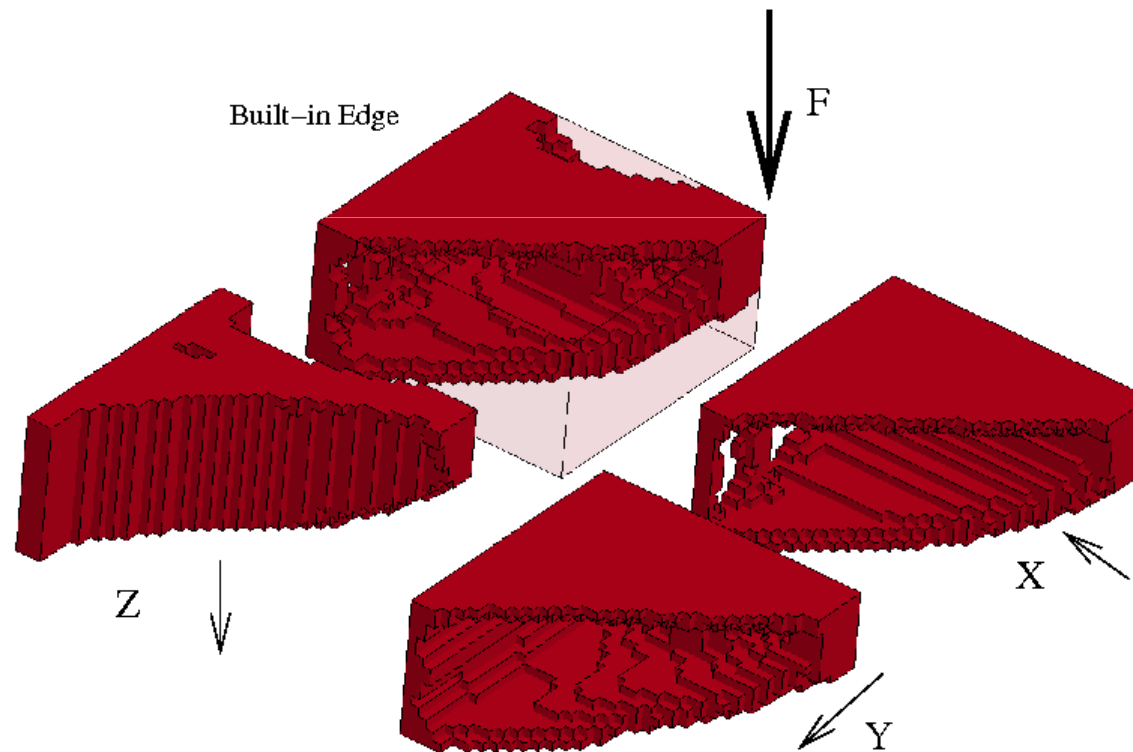
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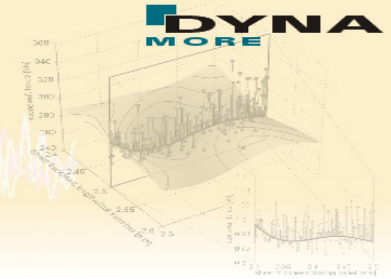
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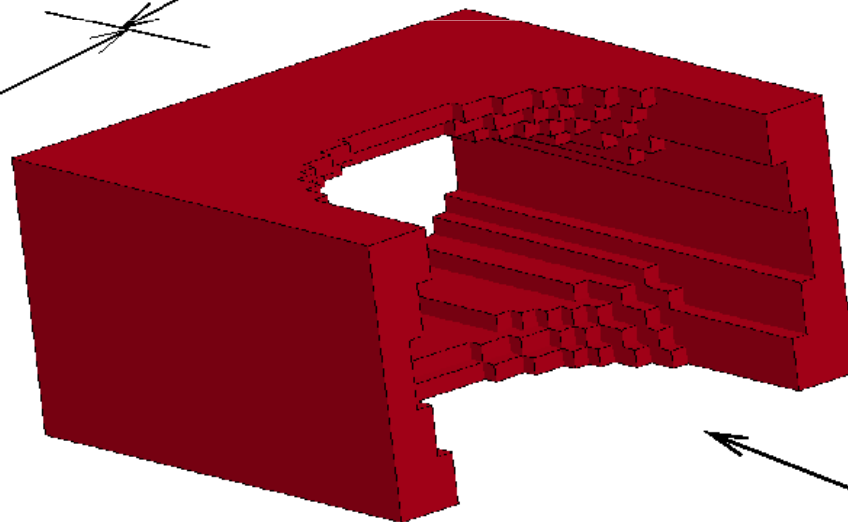
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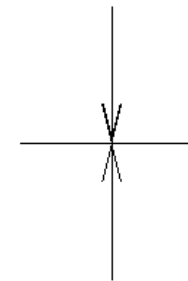
## → LS-OPT/Topology – Outlook Version 2

- Example Symmetry Constraints

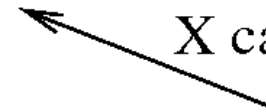
ZX symmetry



XY symmetry

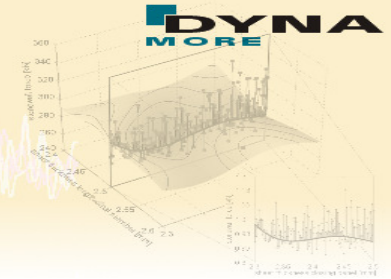


X casting



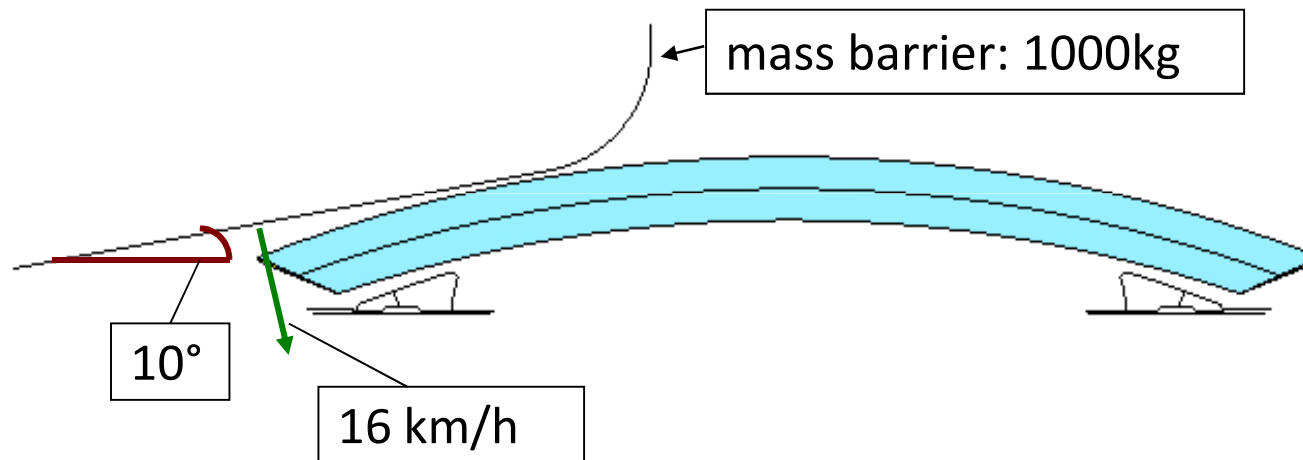
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## → Problem Description

- Optimization of a Crash Management System

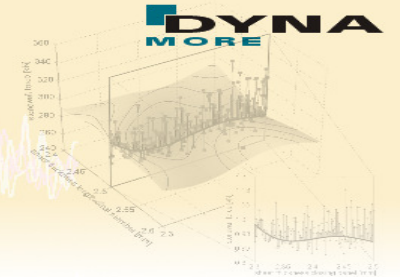


- Objectives are

- *to absorb the impact energy by plastic deformation without exceeding a specific force level*
- *reduce the mass of the bumper*

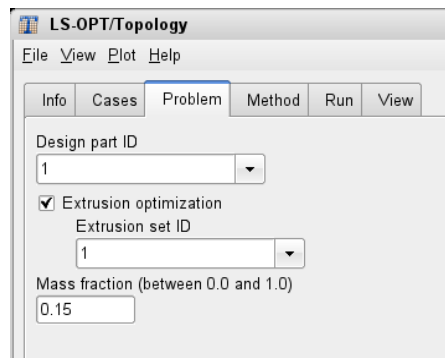
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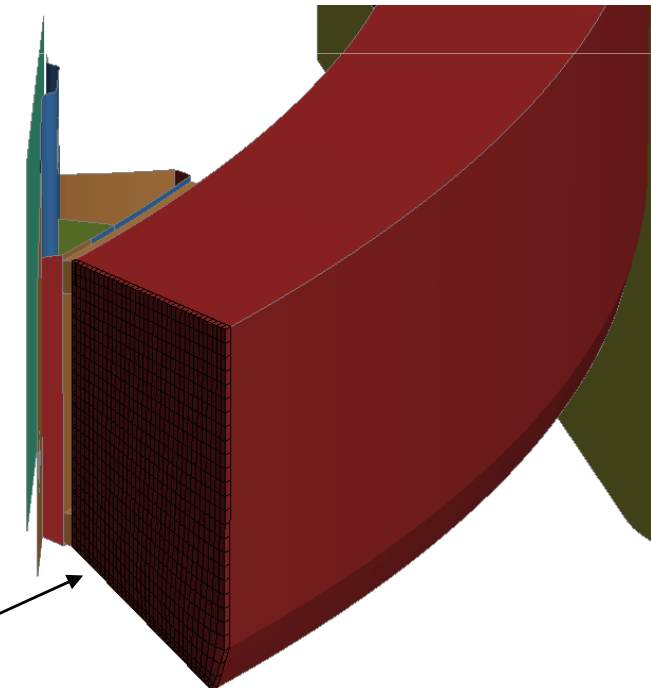


## → Problem Description / Settings

- Installation space for the bumper is defined by an extruded section of solid elements
- In total 565.800 solid elements for the initial model are used
- Mass fraction constraint is set to 15% of the initial (full volume) mass
- An extrusion constraint is introduced by specification of a set of solid elements

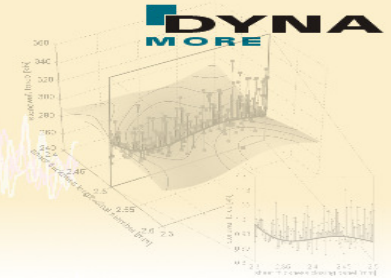


\*SET\_SOLID



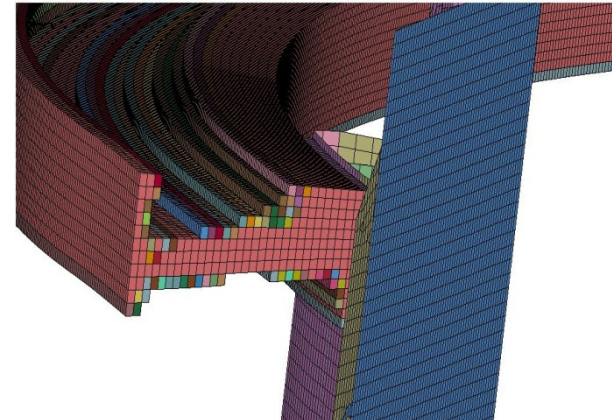
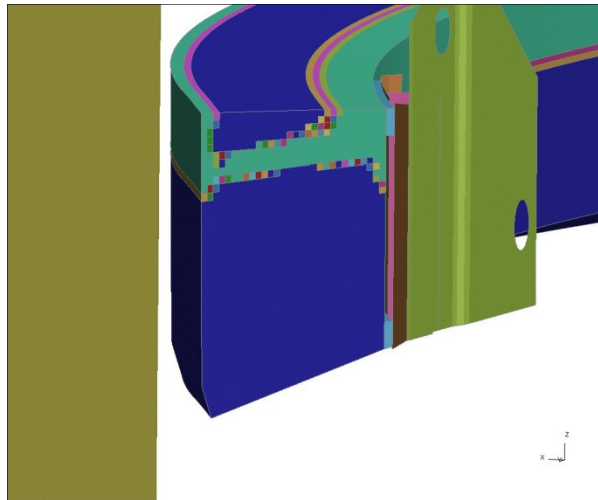
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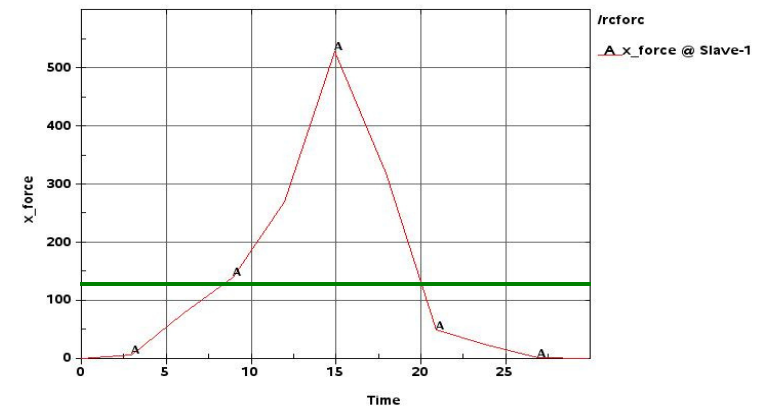


## → Result Topology Optimization

- Result of the topology optimization after 30 iterations, which means 30 LS-DYNA simulations



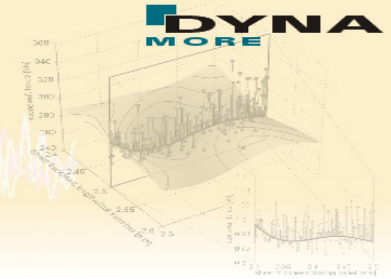
- But contact force is very high and exceeds a required threshold





# Optimization of a Crash Management System

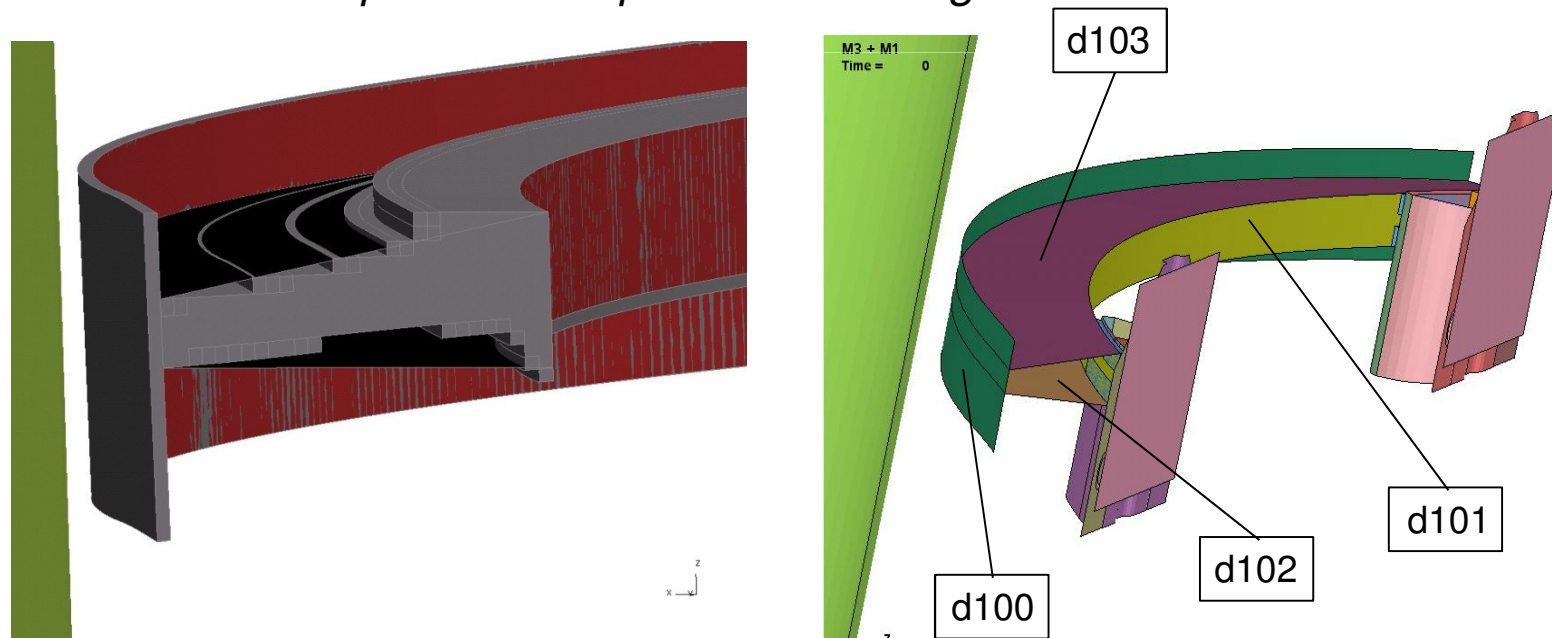
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## → Remodelling from Solids to Shells

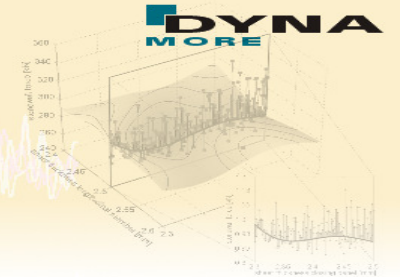
- Introduction of a second stage:

- *re-model the bumper with shell elements considering the results of the topology optimization, and determine optimal sheet thicknesses by constraint parameter optimization using LS-OPT*



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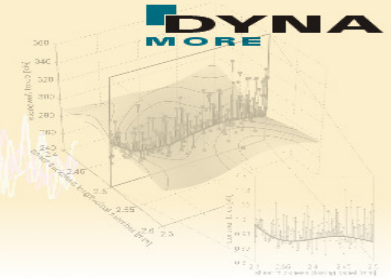


## → Optimization Problem for LS-OPT

- New optimization problem:
  - *Objective is to minimize the mass*
  - *Subject to the constraint*  
 $\max(\text{ContactForce}(t)) < 130\text{kN}$
  - *Variables: Sheet thicknesses of four parts*
- Successive response surface method (SRSM) is applied in LS-OPT

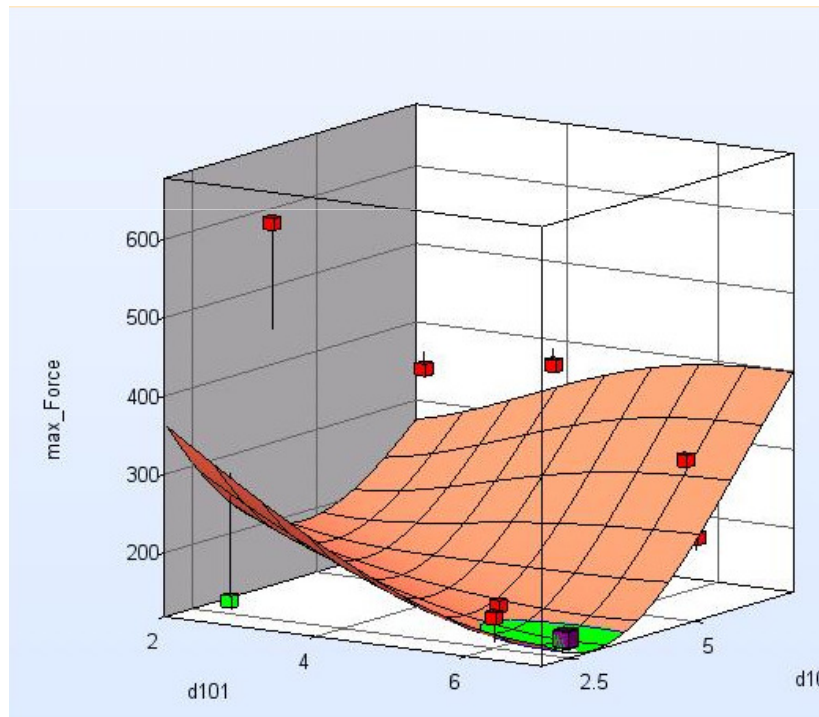
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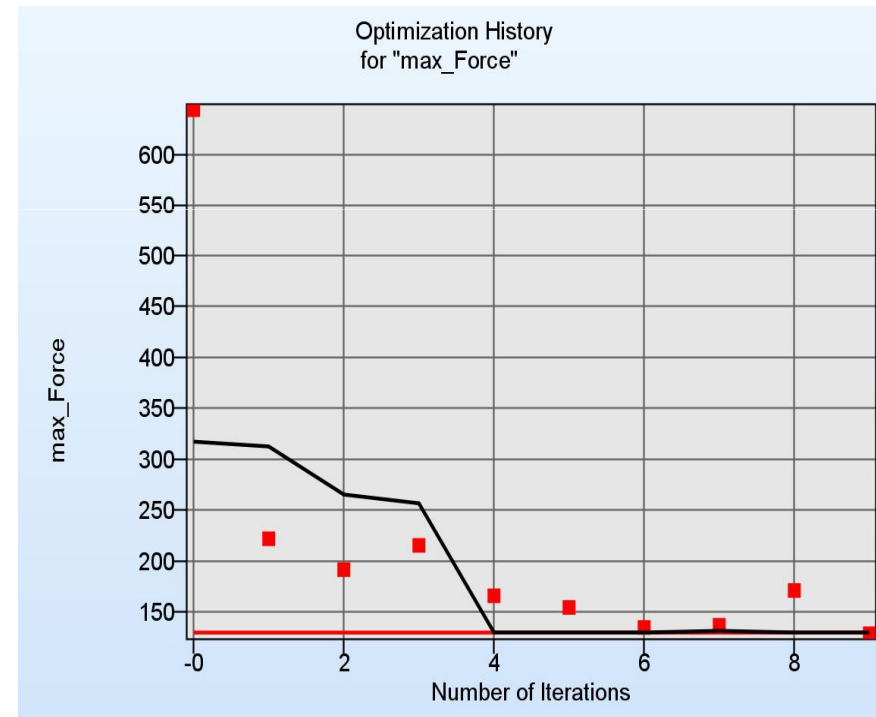


## → Optimization Results

- Result of SRSM Optimization - Convergence after 9 iterations each with 8 runs



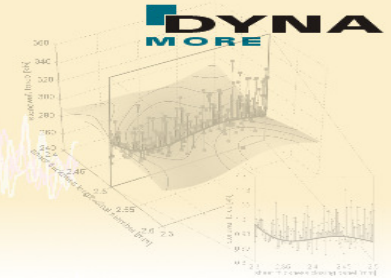
Meta-model used for optimization with feasible and infeasible regions



Optimization history of max contact force

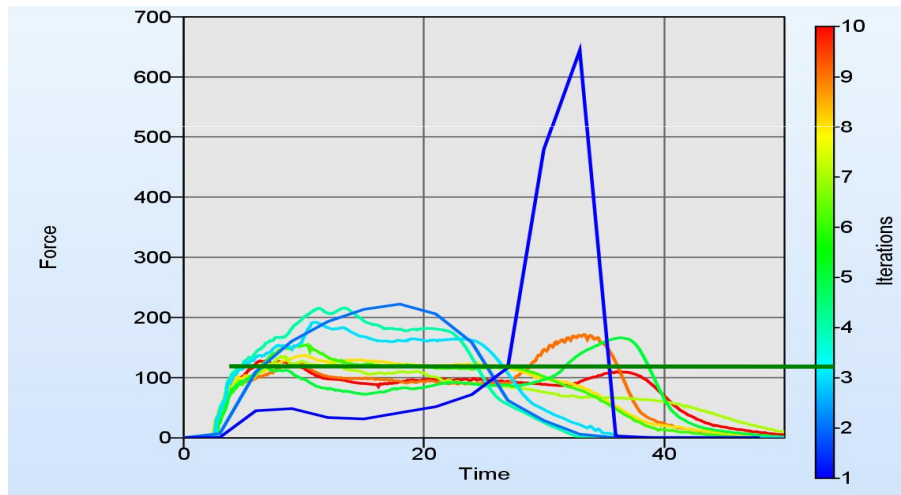
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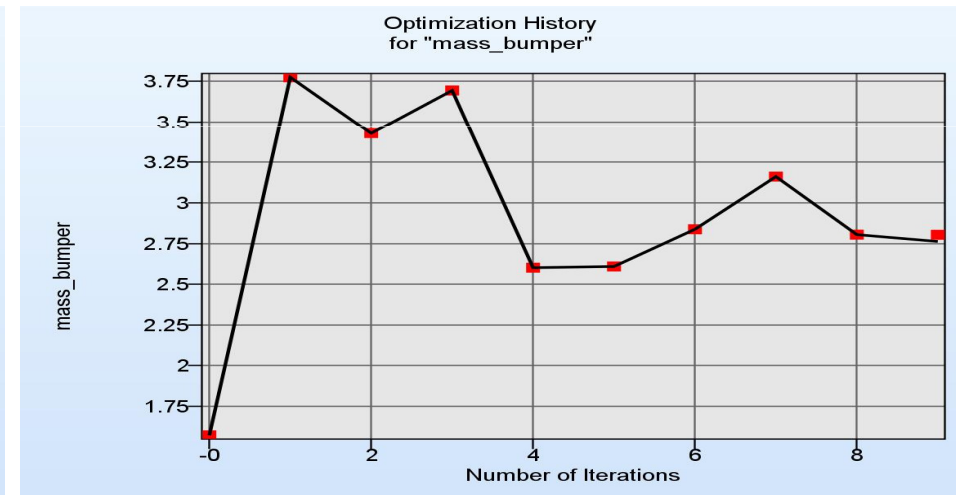


## ➔ Optimization Results

### ■ Result of SRSM Optimization

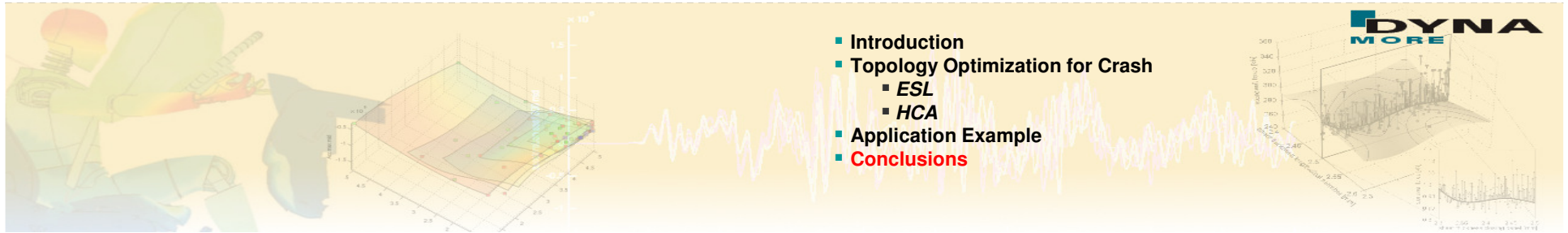


Development of contact force curves during LS-OPT iterations



Optimization history for bumper mass

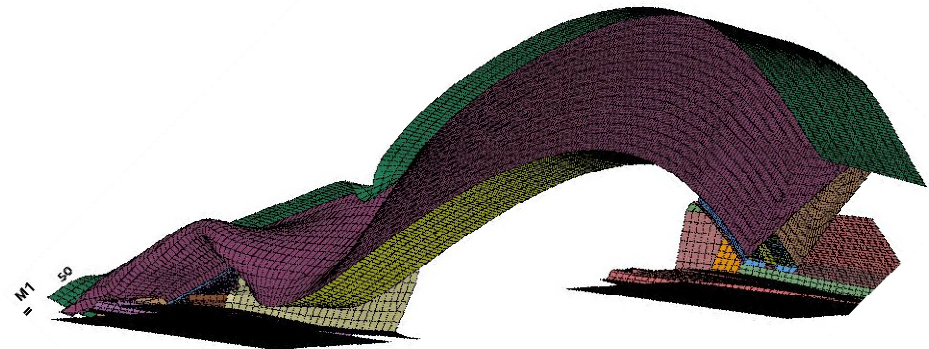




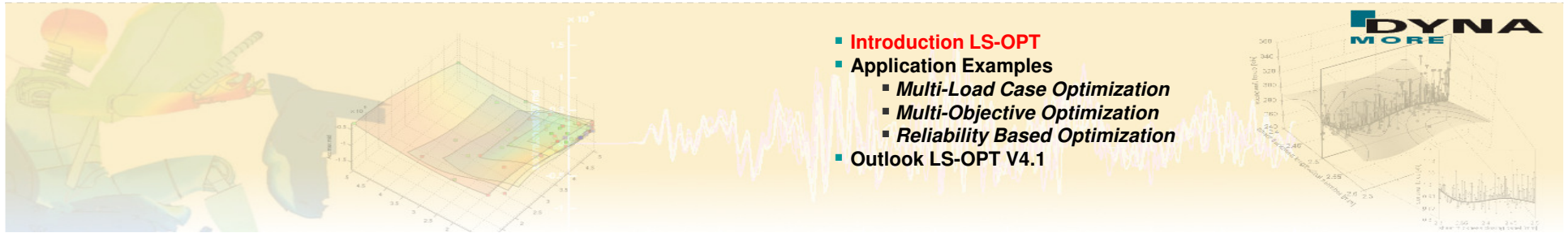
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## ➔ Conclusions

- Optimization has been performed in two steps
  - *Topology optimization with LS-OPT/Topology*
  - *Size optimization with LS-OPT*
- Two step approach was necessary in order to consider a maximum force constraint and it also helps to refine the optimization on the basis of a shell design that represents a feasible design solution.
- Shape optimization on the shell design might be an additional option, but hasn't been addressed in this study







**Thanks for your attention!**

